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**Viana et al.**

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(54) **HIGHLY INTEGRATED SINGLE SUBSTRATE  
MMW MULTI-BEAM SENSOR**

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(List continued on next page.)

(75) Inventors: **Luis M. Viana**, Wakefield, MA (US);  
**Michael Joseph Delcheccolo**, Westford,  
MA (US); **Joseph S. Pleva**,  
Londonderry, NH (US); **Mark E.**  
**Russell**, Westford, MA (US); **Walter**  
**Gordon Woodington**, Lincoln, MA  
(US); **H. Barteld Van Rees**, Needham,  
MA (US); **Stephen P. LeBlanc**,  
Stratham, NH (US)

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(73) Assignee: **Raytheon Company**, Lexington, MA (US)

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**Related U.S. Application Data**

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(51) Int. Cl.<sup>7</sup> ..... **G01S 13/04; G01S 13/93**

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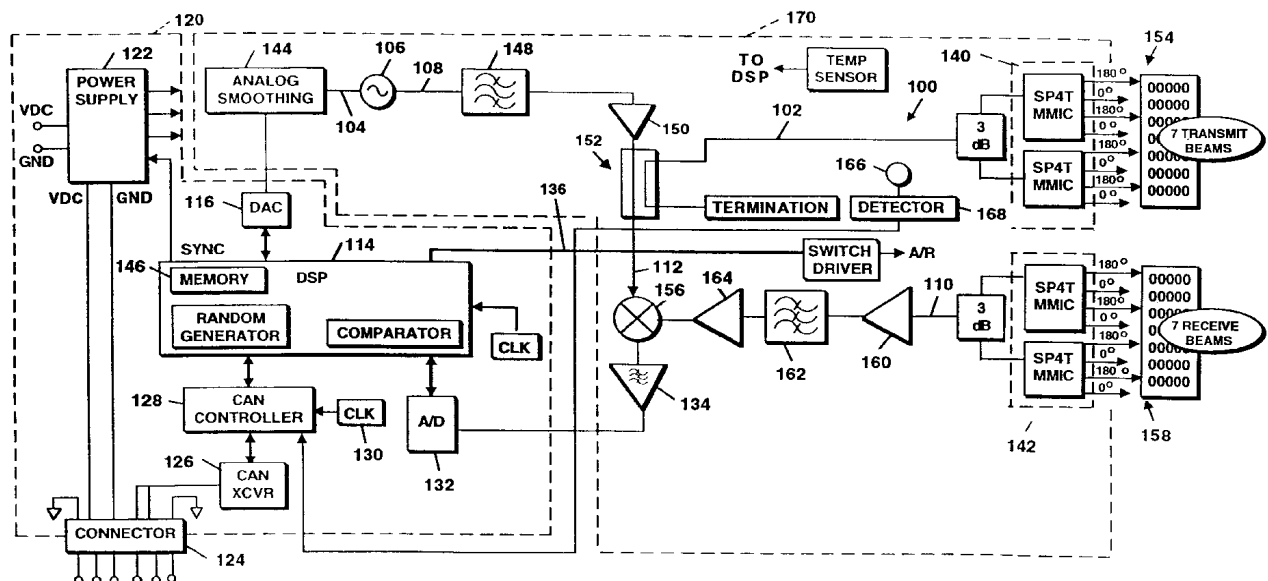
*Primary Examiner*—Bernarr E. Gregory

(74) *Attorney, Agent, or Firm*—Daly, Crowley & Mofford, LLP

(57) **ABSTRACT**

A multiple beam array antenna system comprises a plurality of radiating elements provided from stripline-fed open-ended waveguide coupled to a Butler matrix beam forming network. The Butler matrix beam forming network is coupled to a switched beam combining circuit. The antenna can be fabricated as a single Low Temperature Co-fired Ceramic (LTCC) circuit.

**22 Claims, 9 Drawing Sheets**



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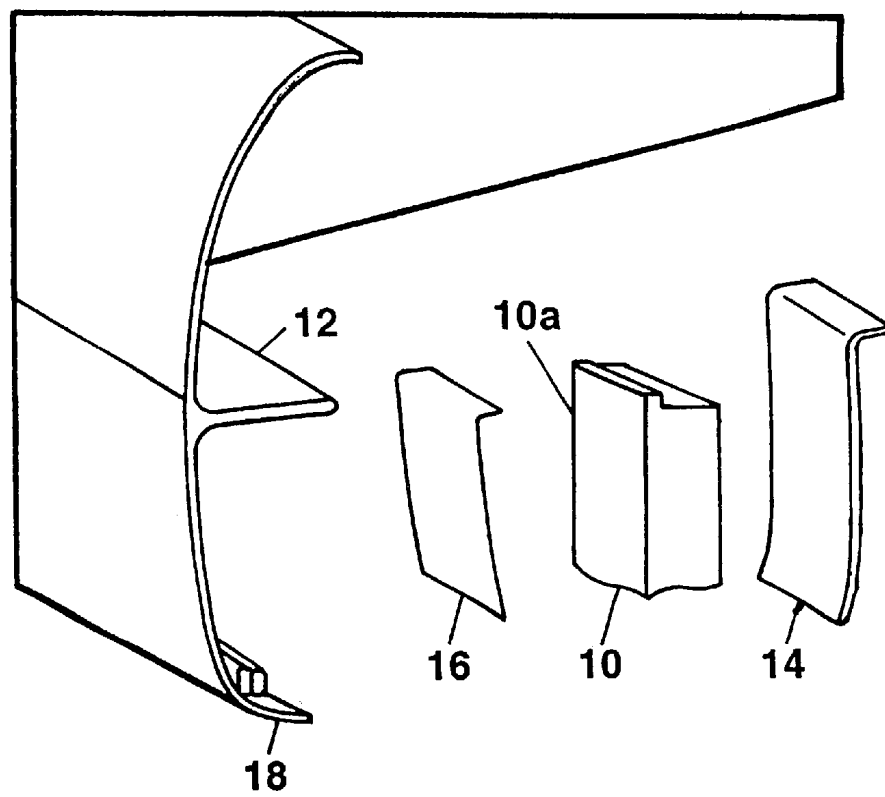
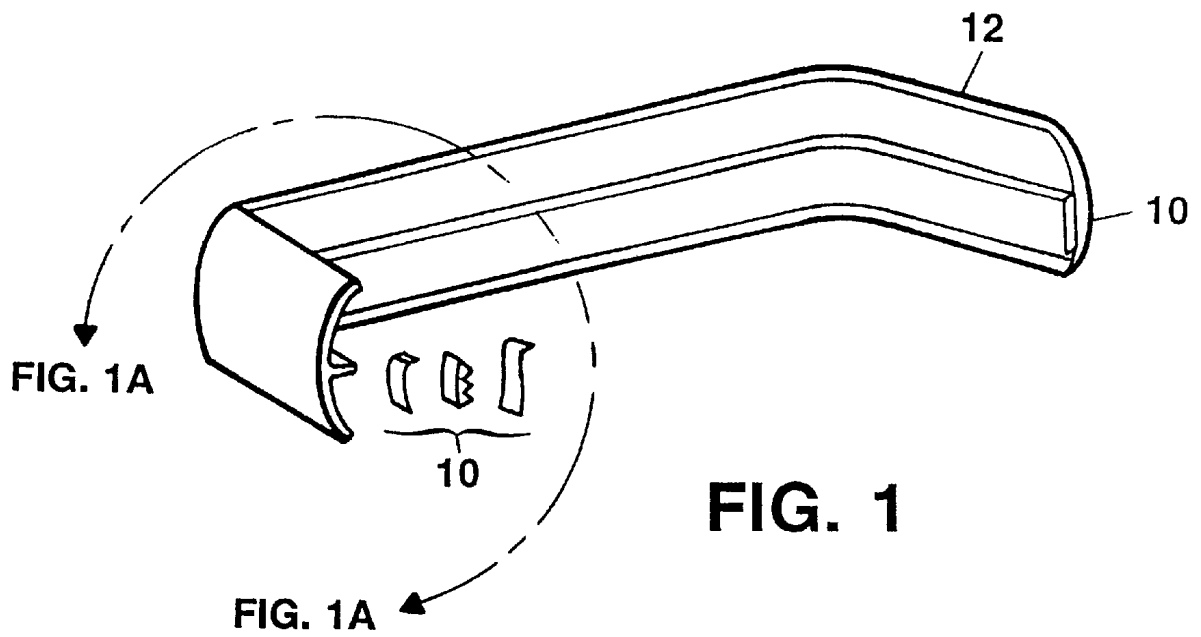
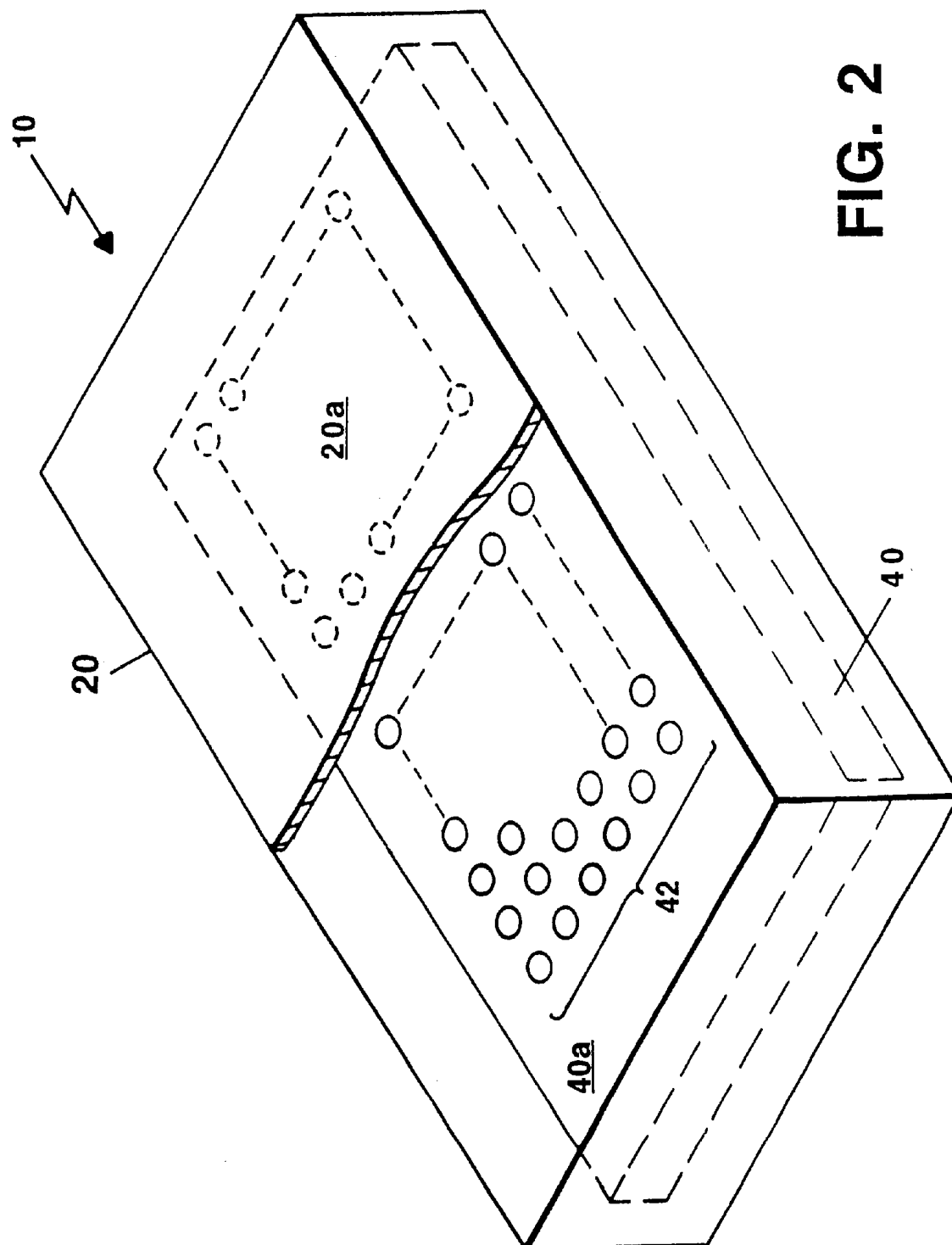
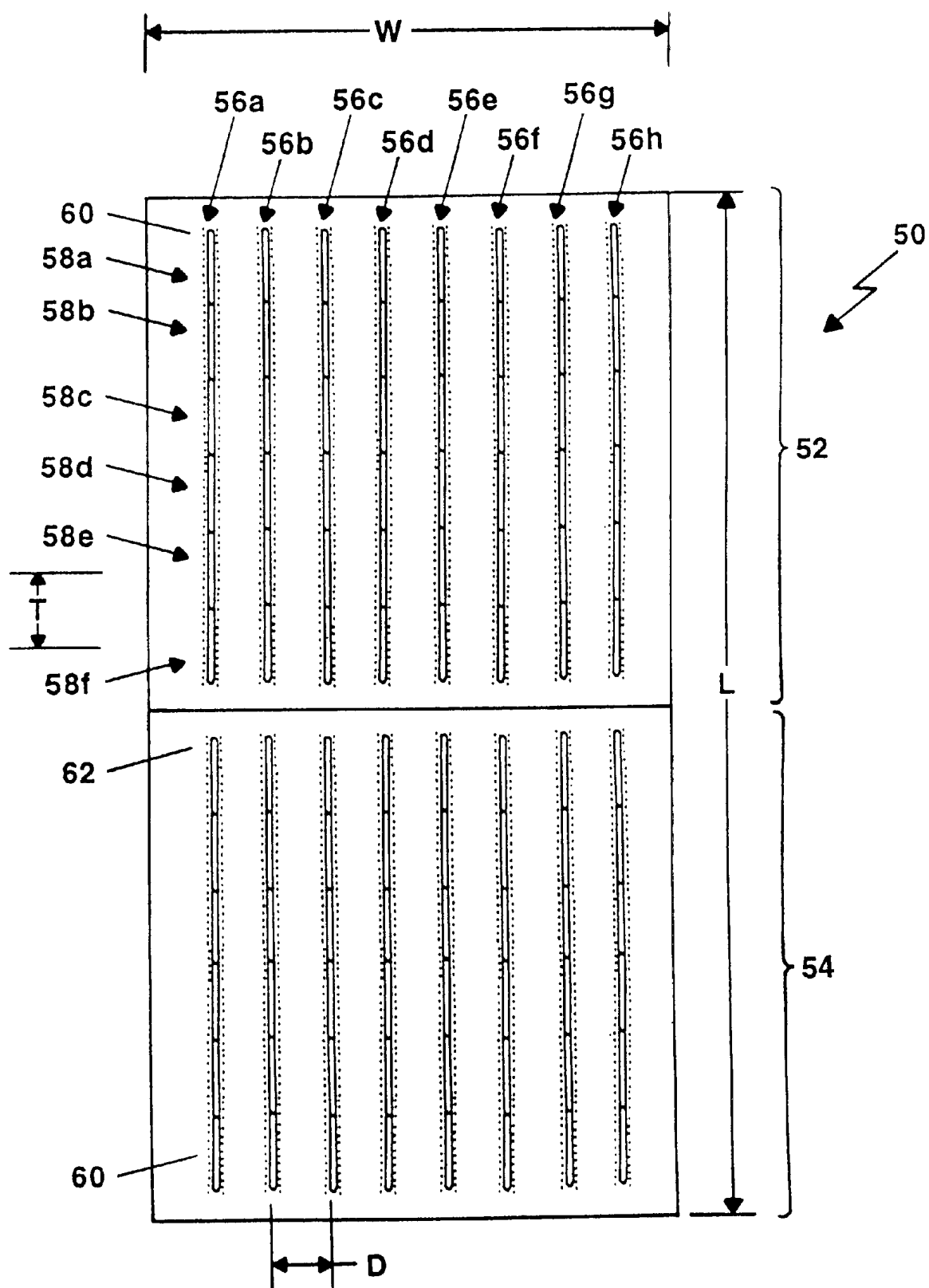
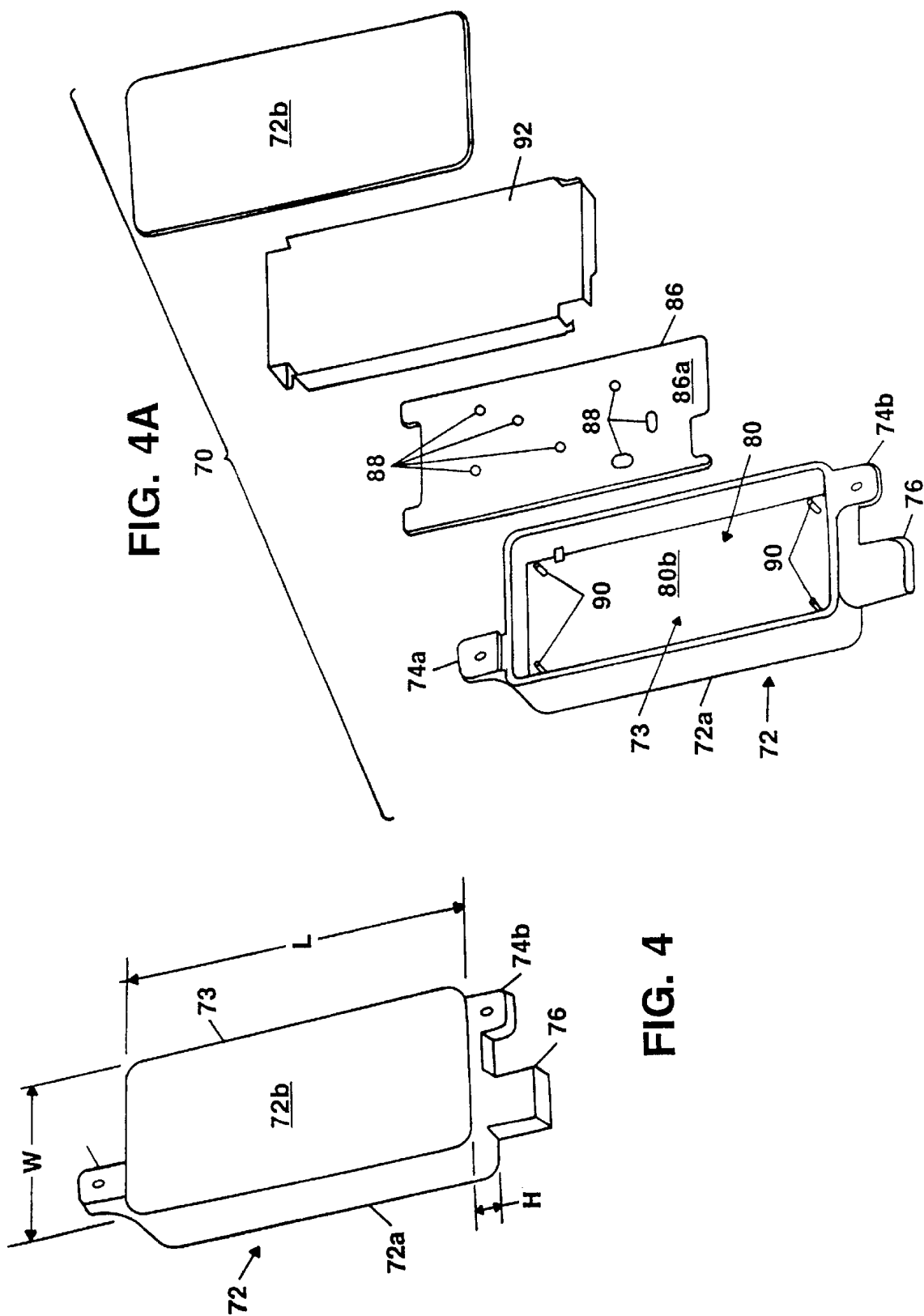


FIG. 1A



**FIG. 2**

**FIG. 3**



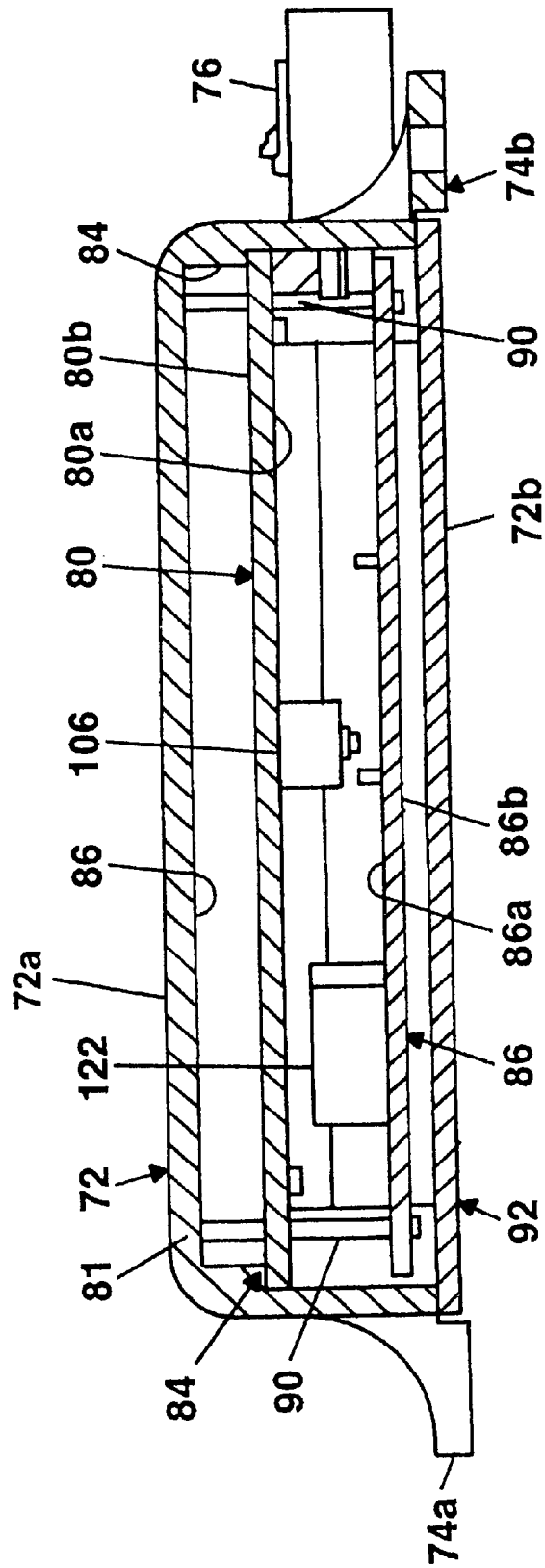
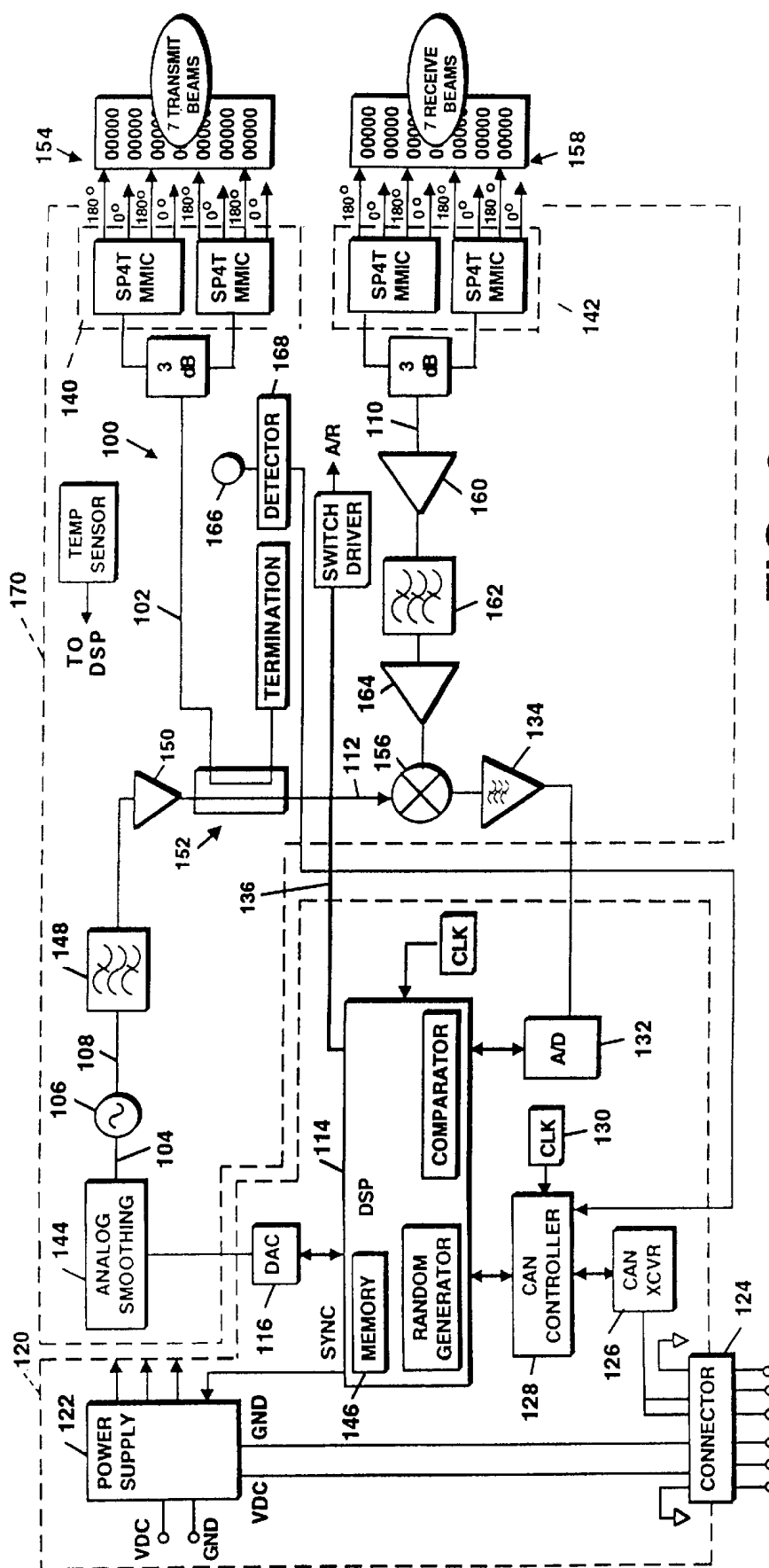


FIG. 5



**FIG. 6**

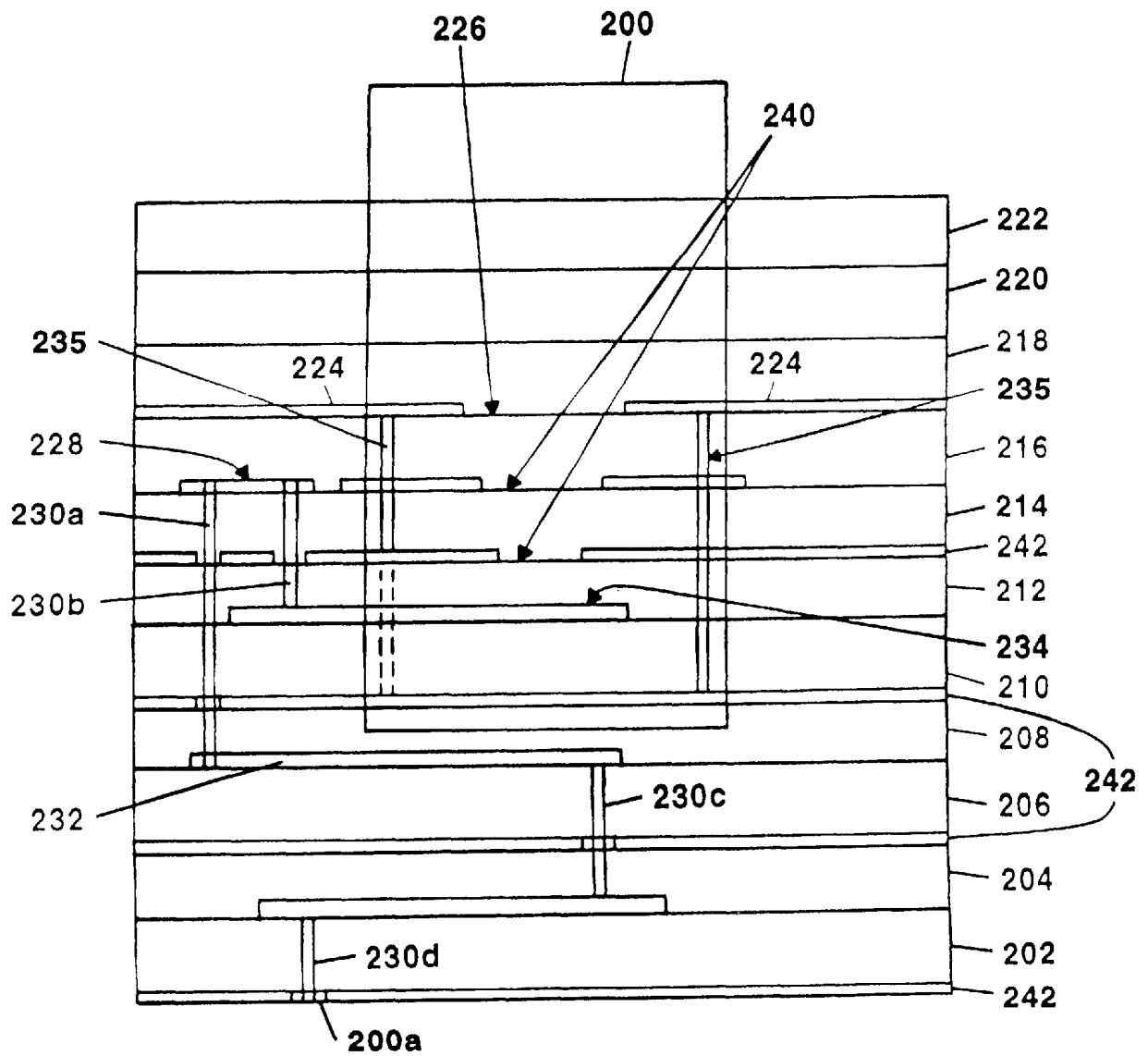
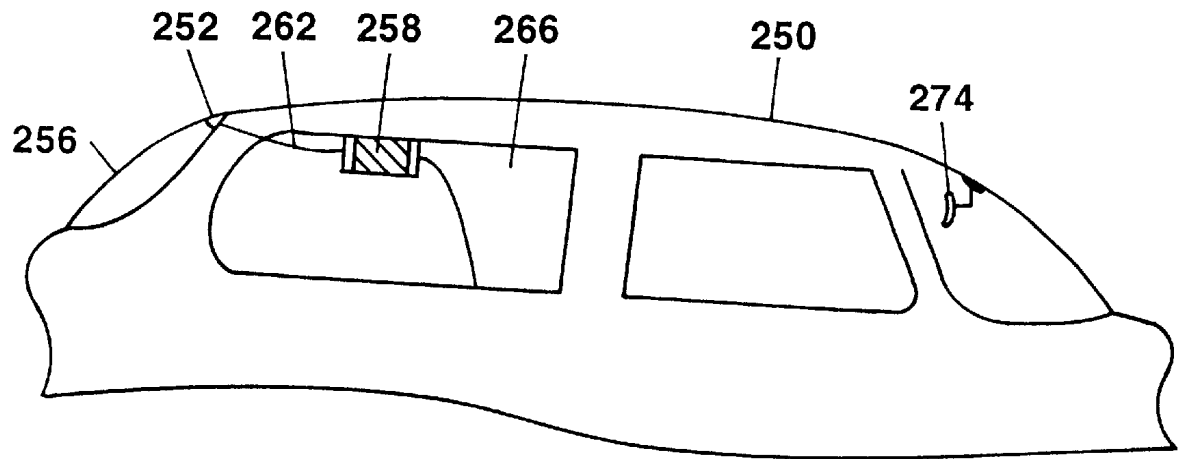
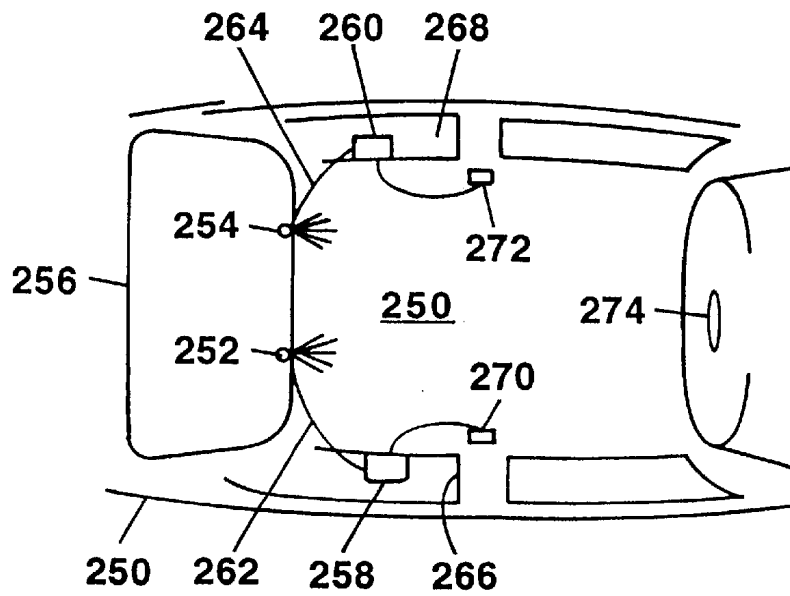


FIG. 7



**FIG. 8A**



**FIG. 8**

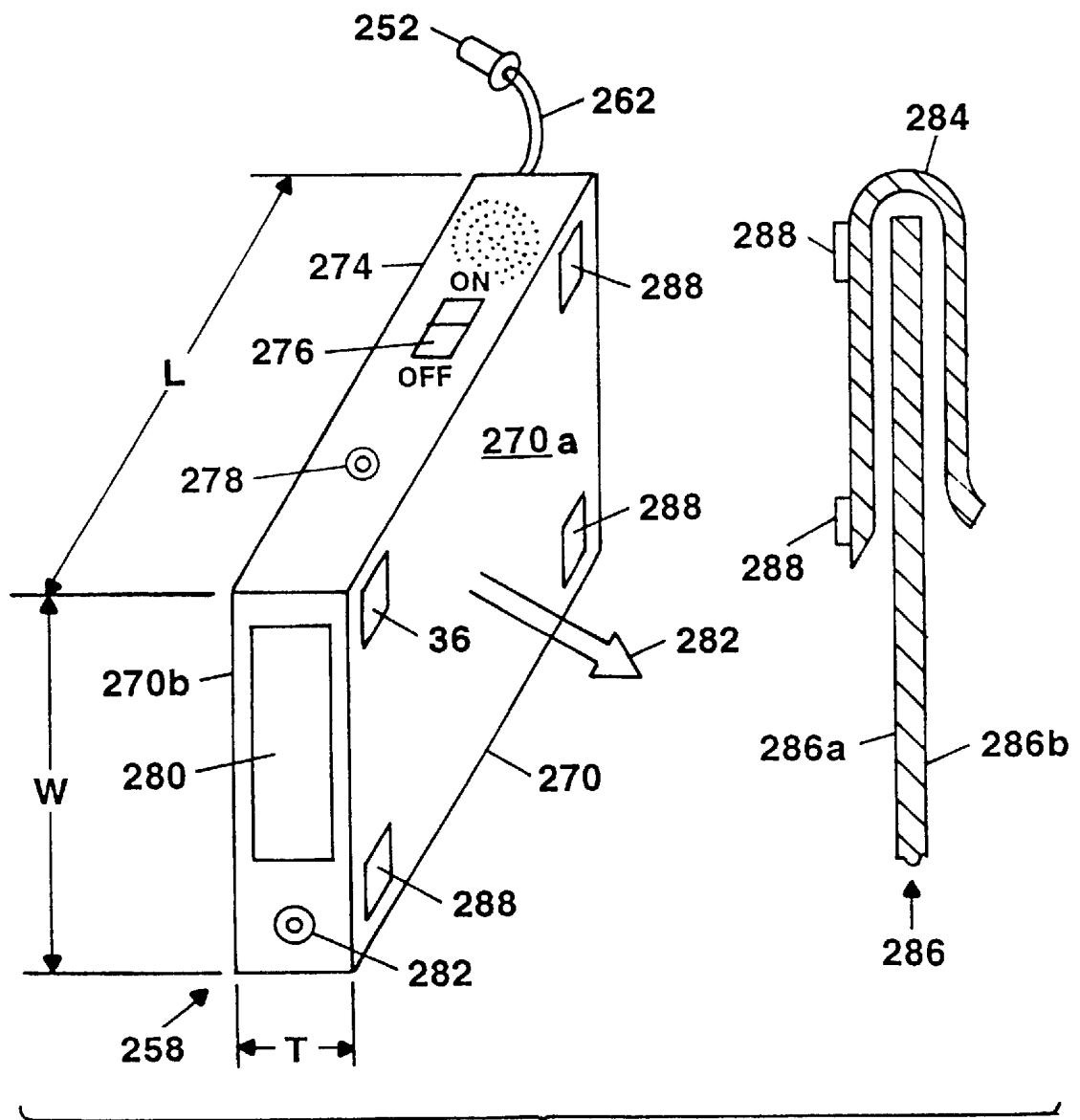


FIG. 9

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## HIGHLY INTEGRATED SINGLE SUBSTRATE MMW MULTI-BEAM SENSOR

### CROSS-REFERENCE TO RELATED APPLICATIONS

This application claims the benefit of U.S. Provisional Application No. 60/226,160, filed on Aug. 16, 2000 which application is hereby incorporated herein by reference in its entirety.

### STATEMENTS REGARDING FEDERALLY SPONSORED RESEARCH

Not applicable.

### FIELD OF THE INVENTION

This invention relates to radar systems and more particularly to high performance, compact, portable radar systems which are field programmable for use in a variety of different applications.

### BACKGROUND OF THE INVENTION

As is known in the art, there is an increasing trend to include radar systems in commercially available products. For example, it is desirable to include radar systems in automobiles, trucks boats, airplanes and other vehicles. Such radar systems must be compact and relatively low cost.

Furthermore, some applications have relatively difficult design parameters including restrictions on the physical size of the structure in addition to minimum operational performance requirements. Such competing design requirements (e.g. low cost, small size, high performance parameters) make the design of such radar systems relatively challenging.

In automotive radar systems, for example, cost and size considerations are of considerable importance. Furthermore, in order to meet the performance requirements of automotive radar applications, (e.g. coverage area) a relatively sophisticated array antenna and radar and transmit circuitry is required.

It would, therefore, be desirable to provide a radar system having relatively high performance characteristics and which is compact, portable and relatively low cost.

### SUMMARY OF THE INVENTION

The present invention provides a millimeter wave (MMW) radar system on a single low temperature ceramic substrate provided from a plurality of Low Temperature Co-fired Ceramic (LTCC) circuit layers. The single LTCC substrate has a top antenna cover or radome layer disposed over an antenna element or radiator layer. The cover or radome layer is used to tune the radiating elements on subsequent radiator layers. MMW transmitter and receiver circuit components are disposed on a second or bottom surface of the single LTCC substrate. Transmitter and receiver circuitry is integrated within the layers of the LTCC substrate to couple the antenna to the transmitter and receiver components. In one embodiment, the antenna is provided from an array of radiating antenna elements embedded in the LTCC substrate with array feed and beam-forming circuitry embedded and integrated throughout the different layers of the LTCC substrate. Transmitter circuit components including but not limited to a voltage controlled oscillator (VCO) and a power amplifier as well as receiver circuit components including but not limited to a low noise

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amplifier (LNA), a mixer and a video amplifier are disposed on the bottom surface of the LTCC substrate. The transmitter and receiver circuit components are coupled to transmit and receive antennas as well as other transmit and receive circuitry through via connections provided in the LTCC substrate. In this manner, a highly integrated, single substrate MMW radar system is provided.

Digital signal processing (DSP), power circuits, control circuits and interface circuits are disposed on a printed wiring board (PWB) which can be coupled to the MMW radar system disposed on the LTCC substrate via a flex cable.

In one embodiment, the LTCC substrate comprising the antenna and MMW transmit and receive circuits is disposed in a housing. The LTCC substrate is disposed in the housing over a first support structure which spaces the antenna aperture a predetermined distance from a first or internal surface of the housing. Also disposed in the housing over a second support structure is the PWB. The second structure spaces a surface of the PWB a predetermined distance from the second surface of the LTCC substrate. Thus, the LTCC substrate and the PWB are disposed in a single common housing. In one embodiment, a flex circuit couples the circuit components disposed on the LTCC substrate to the circuit components disposed on the PWB. Thus the radar is provided as an integrated structure having a relatively connector-less interface. The housing is provided having a single connector through which RF, DC and logic signals are provided. Furthermore, an EMI shield is disposed in the housing to reduce the amount of radiation emitted through the housing from locations other than the antenna aperture. While the integrated single substrate MMW radar of the present invention is particularly well-suited for automotive radar systems, especially active electronically scanned antenna automotive radar systems, it is understood that the radar may also be used in other radar system applications.

### BRIEF DESCRIPTION OF THE DRAWINGS

The foregoing features of this invention, as well as the invention itself, may be more fully understood from the following description of the drawings in which:

FIG. 1 is a partially exploded view of a radar system mounted to a vehicle bumper section;

FIG. 1A is an exploded isometric view of a radar system mounted to a vehicle bumper section;

FIG. 2 is an isometric view of a highly integrated single substrate millimeter wave (MMW) multi-beam sensor system having a portion of a housing removed to reveal an antenna aperture;

FIG. 3 is a top view of an array aperture formed by a plurality of antenna elements;

FIG. 4 is an isometric view of a highly integrated single substrate MMW multi-beam sensor system.

FIG. 4A is an exploded isometric view of a highly integrated single substrate MMW multi-beam sensor system;

FIG. 5 is a cross-sectional view of a highly integrated single substrate MMW multi-beam sensor system of the type shown in FIGS. 1, 2 and 4;

FIG. 6 is a detailed block diagram of a highly integrated single substrate MMW multi-beam sensor system of the type shown in FIGS. 1, 2 and 4;

FIG. 7 is a cross-sectional view of a single substrate which includes and RF antenna, receiver and transmitter circuits;

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FIG. 8 is a top view of a highly integrated single substrate MMW multi-beam sensor system of the type shown in FIGS. 1, 2 and 4 disposed on a vehicle;

FIG. 8A is a side view of the highly integrated single substrate MMW multi-beam sensor system of shown in FIG. 8; and

FIG. 9 is an isometric view of a highly integrated single substrate MMW multi-beam sensor system.

#### DETAILED DESCRIPTION OF THE INVENTION

Referring to FIGS. 1 and 1A, in which like elements are provided having like reference designations, first and second radar systems 10 are mounted behind portions of a vehicle body 12. In this particular example, the vehicle body 12 corresponds to an automobile bumper 16 portion of a vehicle. It should be appreciated, however, that radar system 10 can be mounted behind any portion of a vehicle provided that an appropriate amount of space exists or can be made to accommodate the radar system 10. Radar system 10 can be provided as a highly integrated millimeter wave (MMW) multibeam sensor and thus can be mounted at various locations on a vehicle and is not limited to mounting in association with the bumper 12, as will be described below. Specific techniques for mounting a highly integrated millimeter wave (MMW) multibeam sensor behind a vehicle bumper, fascia, or other vehicle portion are described in U.S. patent application entitled System and Technique for Mounting a Radar System on a Vehicle, filed on Aug. 16, 2001, and assigned Application Ser. No. 09/930,868, assigned to the assignee of the present invention and incorporated herein by reference.

The radar systems 10 may be provided, for example, as the types described in U.S. patent application entitled Radar Transmitter Circuitry and Techniques, filed on Aug. 16, 2001, and assigned Application Ser. No. 09/931,636 and U.S. patent application entitled Switched Beam Antenna Architecture, filed on Aug. 16, 2001, and assigned application Ser. No. 09/932,574, each of which are assigned to the assignee of the present invention and incorporated herein by reference. It should be appreciated of course that other radar systems can be used in accordance with the present invention.

The radar systems 10 are each mounted behind a vehicle section 12 provided from a material which allows radar signal energy to pass therethrough with relatively little, or ideally no, attenuation. The radar system 10 can be coupled to the vehicle body 12 via a mounting bracket 14 or can be coupled directly to the body of the vehicle. A protective barrier section 16 is disposed between an inner wall 18 of the vehicle section 12 and a surface 10a of the sensor 10. The protective barrier section 16 provides additional protection for the sensor 10.

Referring now to FIG. 2, the sensor 10 includes a housing 20 having a portion thereof removed to reveal a single Low Temperature Co-fired Ceramic (LTCC) substrate 40 having a first or top surface 40a on which a plurality of antenna elements 42 are disposed. A preferred antenna array and antenna element for use in automotive radar applications is described in co-pending U.S. patent application entitled "Slot Antenna Element for an Array Antenna" filed Aug. 16, 2001 and assigned application Ser. No. 09/931,633, assigned to the assignee of the present invention and the aforementioned co-pending U.S. patent application entitled "Switched Beam Antenna Architecture" both of the above-referenced applications being incorporated herein by reference in their entirety.

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Also provided in the LTCC substrate 40 is a Butler matrix beam forming circuit, a radiator feed circuit coupled to the antenna elements 42 a plurality of quadrature hybrid and power divider circuits as well as interlayer transition circuits. In one embodiment, the substrate 40 is provided from Ferro's A6-M LTCC tape. The tape is provided having a thickness of about 0.010 inch pre-fired and about 0.0074 inch post-fired and a relative dielectric constant of about 5.9. The LTCC tape has a loss characteristic at 24 GHz of 1.1 dB per inch for a 0.0148 inch ground plane spacing. In other embodiments, the tape layers can be provided from Ferro's A6-S tape.

The single substrate 40 is provided from LTCC for a variety of reasons including but not limited to its potential for low cost in high volume production. Furthermore, LTCC allows compact circuit design and is compatible technology at this frequency for multi-layer circuits with large quantities of reliable, embedded vias (approximately 1200 vias in one particular embodiment). Surface-mount devices can also be integrated with LTCC as will be described below in conjunction with FIGS. 4, 5 and 7 below.

Referring now to FIG. 3, an array antenna 50 having a length L and a width W includes a transmit array 52 and a receive array 54. Each of the arrays 52, 54 includes eight rows 56a-56g and six columns 58a-58f. Thus, each of the transmit and receive arrays 52, 54 have forty-eight radiating elements (or more simply "radiators" or "elements"), generally denoted 60, with eight elements in azimuth and six elements in elevation. The array antenna 50 may be provided, for example, on the surface 40a (FIG. 2) in the LTCC substrate 40 (FIG. 2).

As described in detail in the above-mentioned U.S. patent applications entitled "Slot Antenna Element for an Array Antenna," application Ser. No. 09/931,633, filed on Aug. 16, 2001 and "Switched Beam Antenna Architecture," application Ser. No. 09/932,574, filed on Aug. 16, 2001 each radiating element 60 is a stripline-fed open-ended cavity in LTCC. The cavity is formed in the LTCC 40 (FIG. 2) using embedded vias, generally denoted 62, that create the "cavity walls." Each of the arrays 52, 54 have a rectangular lattice spacing: 0.223" (azimuth) x 0.295" (elevation). The azimuth spacing is selected to be compatible with a Butler matrix feed circuit selected to yield desired beam locations which provided desired detection zones. The elevation spacing is selected to achieve a desired elevation beamwidth and the maximum spacing needed to avoid a cover induced scan blindness.

In an automotive radar application, the antenna 50 is enclosed in the housing 12 (FIG. 2) and radiates through the housing cover 12a (FIG. 2). In some embodiments, the cover 12 is incorporated into the radiator design while in other embodiments the cover is spaced from the antenna aperture by a distance corresponding to one-half wavelength.

Referring now to FIGS. 4, 4A and 5 in which like elements are provided having like reference designations throughout the several views, a highly integrated MMW multi-beam sensor system 70 includes a housing 72 having a pair of mounting ears 74a, 74b and a connector 76 projecting therefrom. RF, DC and logic signals are provided to and from the sensor 70 via the connector 76. In one embodiment, the housing 72 is provided having a length L typically of about 120 mm, a width W typically of about 66 mm, and a height H typically of about 32 mm and all signals provided to and from the sensor 70 are provided through the connector 76 to a car area network (CAN) controller as will be described below in conjunction with FIG. 6.

The housing **72** includes a base portion **72a** and a cover portion **72b**. In this particular embodiment, the base portion **72a** is provided having integral sides to thus provide a recess region **73** within the base **72a**. The base **72a** may be provided using injection molding techniques of any other technique well known to those of ordinary skill in the art of providing structurally sound, compact and lightweight structures.

The base **72a** side walls have a support structure **84** projecting therefrom. In one particular embodiment, the support structure **84** corresponds to a shoulder region **84** of the base **72a**. Also projecting from a surface of base **72a** is a second support structure here provided from a plurality of posts **90**. In this particular embodiment, the posts **90** project from a bottom surface of the base **72a**.

An LTCC substrate **80** having first and second opposing surfaces **80a**, **80b** (**80b** not visible in FIG. 4) is disposed in the recess region **73** of the base **72a**. An antenna, which may be provided for example as the type described above in conjunction with FIG. 3 is disposed on surface **80b**. The antenna on the substrate **80** is thus disposed to transmit and receive signals through the bottom surface of base **72a**. The LTCC substrate **80** is disposed in the recess region **73** and supported on the shoulder portion **84** provided in the base **72a**. The shoulder region **84** is provided to support the substrate **80** and space the aperture of the antenna provided on the LTCC substrate **80** a predetermined distance from a surface of the housing portion **72a** as will be described in more detail below in conjunction with FIG. 5.

A printed circuit board (PCB) **86** having first and second opposing surfaces **86a**, **86b** is also disposed in the recess region **73** of the housing **72**. PCB **86** is adapted to have circuit components **88** including but not limited to surface mounting circuit components disposed on the opposing surfaces **86a**, **86b**. The circuit components **88** may be provided as inductors, power supplies and digital circuit components and subsystems.

The PWB **86** is also disposed in the recess region **73** and is supported by spacers **90**. The spacers **90** are selected to space a first surface of the PWB **86** a predetermined distance from the surface **80a** of the LTCC substrate **80**. The particular distance by which PWB **86** is spaced from LTCC substrate **80** is selected such that the circuit components disposed on the surface **80a** of substrate **80** do not interfere with either circuit components **88** disposed on the surface **86b** of PWB **86** or with the surface **86b** itself.

An EMI shield **92** is disposed over the PWB **86** and provides a barrier which prevents leakage of substantially all radiation from the LTCC substrate **80** and the circuits provided therewith as well as PWB **86** and the circuits provided therewith. The shield **92** also provides a level of immunity from radiated emissions coming from outside the sensor **70**. The cover **72b** is provided having a thickness selected to allow attachment to the base **72a** via a vibrational technique.

Referring now to FIG. 6, a radar system which may be similar to the radar systems described above in conjunction with FIGS. 1 and 2 respectively for use as a side object detection (SOD) system in an automotive radar application is shown in greater detail. In general overview of the operation of a transmitter **100**, the FMCW radar transmits a signal **102** having a frequency which changes in a predetermined manner over time. The transmit signal **102** is generally provided by feeding a VCO control or ramp signal **104** to a voltage controlled oscillator (VCO) **106**. In response to the ramp signal **104**, the VCO **106** generates a chirp signal **108**.

A measure of transmit time of the RF signal can be determined by comparing the frequency of a received or return signal **110** with the frequency of a sample **112** of the transmit signal. The range determination is thus provided by measuring the beat frequency between the frequencies of the sample **112** of the transmit signal and the return signal **110**, with the beat frequency being equal to the slope of the ramp signal **104** multiplied by the time delay of the return signal **110**.

The measured frequency further contains the Doppler frequency due to the relative velocity between the target and the radar system. In order to permit the two contributions to the measured frequency shift to be separated and identified, a CW tone is generated after the chirp so that the return signal from it differs solely by the Doppler frequency.

In one embodiment, the VCO control signal **104** is generated with digital circuitry and techniques. In a preferred embodiment, the ramp signal **104** is generated by a DSP **114** and a digital-to-analog converter (DAC) **116**. Use of the DSP **114** and DAC **116** to generate the ramp signal **104** is possible in the SOD system of FIG. 6 since, it has been determined that by proper selection of the detection zone characteristics including but not limited to detection zone size, shape and resolution, precise linearity of the chirp signal **108** is not necessary. With this arrangement, the frequency of the transmit signal **102** is accurately and easily controllable which facilitates implementation of several features. As one example, one or more characteristics of successive ramps in the ramp signal **104** are randomly varied in order to reduce interference between similar, proximate radar systems. As another example, temperature compensation is implemented by appropriately adjusting the ramp signal **104**. Yet another example is compensation for non-linearity in the VCO operation. Further, changes to the SOD system which would otherwise require hardware changes or adjustments can be made easily, simply by downloading software to the DSP **114**. For example, the frequency band of operation of the SOD system can be readily varied, as may be desirable when the SOD is used in different countries with different operating frequency requirements.

An electronics portion **120** of the SOD system includes the DSP **114**, a power supply **122** and a connector **124** through which signal buses are coupled between the SOD system and a vehicle on which the SOD system is disposed. A digital interface unit is provided in the form of a controller area network (CAN) transceiver (XCVR) **126** which is coupled to the DSP **114** via a CAN microcontroller **128**. The CAN controller **128** has a system clock **130** coupled thereto to provide frequency stability. In one embodiment, the system clock is provided as a crystal controlled oscillator. An analog-to-digital (A/D) converter **132** receives the output of a video amplifier **134** and converts the signal to digital form for coupling to the DSP **114** for detection processing. In one embodiment, the A/D converter **132** is provided as a twelve bit A/D converter. Those of ordinary skill in the art will appreciate, however, that any A/D converter having sufficient resolution for the particular application may be used. A signal bus **136** is coupled to antenna switch circuits **140**, **142** in order to provide control signals to drive the switches which comprise the switch circuits. Also provided in the electronics portion **120** of the SOD system is a memory in which software instructions, or code and data are stored. In the illustrative embodiment of FIG. 6, the memory is provided as a flash memory.

The DSP provides output signals, or words to the DAC which converts the DSP output words into respective analog signals. An analog smoothing circuit **144** is coupled to the

output of the DAC in order to smooth the stepped DAC output to provide the ramp control signal to the VCO. The DSP includes a memory device **146** in which is stored a look-up table containing a set of DSP output signals, or words in association with the frequency of the transmit signal generated by the respective DSP output signal.

The VCO **106** receives ramp signal **104** from the analog smoothing circuit **144**. In one embodiment, the VCO operates in the transmit frequency range of between 24.01 to 24.24 GHz and provides an output signal to bandpass filter **148**, as shown.

The output of the VCO **106** is filtered by the bandpass filter **148** and amplified by an amplifier **150**. A portion of the output signal from amplifier **150**, is coupled via coupler **152** to provide the transmit signal **102** to a transmit antenna **154**. Another portion of the output signal from the amplifier **150** corresponds to a local oscillator (LO) signal fed to an LO input port of a mixer **156** in the receive signal path.

The switch circuits **140**, **142** are coupled to the receive and transmit antennas **154**, **158** through a Butler matrix (not shown in FIG. 6). The antennas **154**, **158** and switch circuits **140**, **142**, and Butler matrix can be of the type described in the above-referenced patent applications entitled Slot Antenna Element for an Array Antenna and Switched Beam Antenna Architecture. Suffice it here to say that the switch circuits and Butler matrix operate to provide the antenna having a switched antenna beam with antenna beam characteristics which enhance the ability of the SOD system to detect targets.

The received signal **110** is processed by an RF low noise amplifier (LNA) **160**, a bandpass filter **162**, and another LNA **164**, as shown. The output signal of the RF amplifier **164** is down-converted by mixer **156** which receives the local oscillator signal coupled from the transmitter, as shown. Illustrative frequencies for the RF signals from the amplifier **164** and the local oscillator signal are on the order of 24 GHz. Although the illustrated receiver is a direct conversion, homodyne receiver, other receiver topologies may be used in the SOD radar system.

The video amplifier **134** amplifies and filters the down-converted signals which, in the illustrative embodiment have a frequency between 1 KHz and 40 KHz. The video amplifier may incorporate features, including temperature compensation, filtering of leakage signals, and sensitivity control based on frequency, as described in a co-pending U.S. patent application entitled "Video Amplifier for a Radar Receiver," application Ser. No. 09/931,593, filed on Aug. 16, 2001, and incorporated herein by reference in its entirety.

The A/D converter **132** converts the analog output of the video amplifier **134** into digital signal samples for further processing. In particular, the digital signal samples are processed by a fast Fourier transform (FFT) within the DSP in order to determine the content of the return signal within various frequency ranges (i.e., frequency bins). The FFT outputs serve as data for the rest of the signal processor **262** in which one or more algorithms are implemented to detect objects within the field of view, as described in co-pending U.S. patent application entitled "Radar Transmitter Circuitry and Techniques," application Ser. No. 09/931,636, filed on Aug. 16, 2001, and incorporated herein by reference in its entirety.

The radar system includes a temperature compensation feature with which temperature induced variations in the frequency of the transmit signal are compensated by adjusting the ramp signal accordingly. For this purpose, the transmitter **100** includes a DRO **166** coupled to a microwave

signal detector **168**. The output of the microwave detector is coupled to an analog-to-digital converter of the CAN controller **128** for processing by the DSP **114**. The details of such processing are described in the aforementioned U.S. patent application Ser. No. 09/931,636, filed Aug. 16, 2001, entitled "Radar Transmitter Circuitry and Techniques."

In one embodiment, the apertures of the transmit and receive antenna array **154**, **158** form surface **80a** of the LTCC substrate **80**. The RF circuit components which provide the RF transmitter and receiver components denoted **170** are all included either within or on the LTCC substrate **80**. For example, filter **148**, coupler **152** and various printed circuit transmission lines provided within the layers of the substrate **80** as will be described below in conjunction with FIG. 7.

VCO **106** is provided as a surface mount component disposed on a surface of the substrate **80**. Similarly amplifiers **150**, **160**, **164** and mixer **156** may all be provided as monolithic microwave integrated circuits (MMICs) and disposed on a surface of the substrate **80**.

Similarly, those components which comprise electronics portion **120** are disposed on the PWB **86**. For example, DSP **114**, DAC **116**, power supply **122**, LAN XCVR and controller **126**, **128** and AD **132** are all disposed on first or second surfaces **86a**, **86b** of the PWB **86**. In this manner, the sensor **70** is provided as an entire radar system in a compact package.

Referring now to FIG. 7, a radiating element **200** and associated feed circuits are provided from twelve 0.0074" tape LTCC layers **202-222** with a (stripline) ground plane spacing of 0.0148."

The radiating element **200** itself is provided from layers **210-222** as shown. It should be noted that cover layers **218-222** are integral to the element **200**. Layer **216** has a ground plane **224** disposed thereon. Portions of the ground plane are removed to form an aperture **226**.

A power divider circuit **228** is coupled through conductive vias **230a**, **230b** to a conductive trace **232** and a strip line feed circuit **234**, respectively. Thus, an elevation feed circuit is interlaced with the element **200**.

Capacitive windows **240** are formed on layers **214**, **216** via by disposing ground planes material on the layers **214**, **216** and providing openings in the ground planes. Layers **202**, **204** and **208** are also provided having ground planes **242** disposed thereon. Layers **202-208** are dedicated to a Butler Matrix circuit while layers **210-216** are dedicated to the radiator and feed circuit.

A plurality of embedded vias **235** in the LTCC are used for forming the waveguide structure of the radiator in the LTCC while vias **230a**, **230b** are used for transitioning between the circuits on the different layers. The embedded vias **235** form a waveguide structure and share the same layers as the power divider circuit **228** and the radiator feed circuit **234**.

The LTCC manufacturing flow comprises eight generic operations which are defined as: tape blanking, via formation, via filling, conductor deposition, lamination, wafer firing, continuity test, and dicing. The following is a brief description of each of the eight core work centers.

Raw LTCC is supplied in tape form on spools having a standard width of either 7" or 10". Typical tape area per roll ranges from 4200 to 6000 sq. in. and is also predetermined at time of order. The blanking of LTCC tape is performed manually with the use of an arbor blanking die. Tape is blanked to either a 5" or a 7" manufacturing format size. An orientation hole is also introduced during the blanking

operation which references the LTCC tape's ascast machine and transverse directions. This orientation hole will ultimately allow for layers to be identified and cross-plied in order to optimize total product shrinkage at firing.

The creation of Z-axis via holes is performed through the use of a high speed rapid punch system. The system is driven by punch CAD/CAM data which is electronically down loaded via Ethernet directly to the manufacturing work cell. The supplied punch files contain X- Y-coordinate locations for via formation. Individual tape layers, in either a 5" or 7" format, are mounted into single layer tape holders/frames. These framed layers are subsequently loaded into a handling cassette which can house a maximum of 25 LTCC tape layers. The cassette is loaded and is handled automatically at the work center when respective punch programs are activated. The high speed punch processes via holes in tape layers individually and ultimately indexes through the entire cassette. Via holes are formed at typical rates of 8 to 10 holes per second. At the completion of via formation for a particular tape layer the cassette is unloaded from the work center, processed tape layers removed, and the cassette is reloaded for continued processing.

LTCC tape layers which have completed respective via formation operations require the insertion of Z-axis conductors in order to ultimately establish electrical interface with upper and lower product layers. The via filling operation requires the use of positive pressure displacement techniques to force conductive pastes into via formed holes in the dielectric tape. Mirror image stencils are manufactured for respective tape layers which feature all punched via hole locations; these stencils are fixtured on a screen printing work cell. LTCC tape layers are soft fixtured onto a porous vacuum stone. The stone is indexed under the stencil where a preset pressure head travels over the stencil forcing deposited conductor paste through the stencil and into the dielectric tape. Each tape layer is processed in a similar fashion; all layers are dried, driving off solvents, prior to follow on operations.

Via filled dielectric tape layers require further processing to establish X- and Y-axis conductor paths. The deposition of these conductor mediums provides "from-to" paths on any one LTCC layer surface and originate from and terminate at filled via locations. The conductor deposition operation employs the same work center as described in the via filling operation with the exception that wire mesh, emulsion patterned screens are substituted for through hole stencils. The technique for fixturing both the screen and the tape product is also the same. All product layers are serially processed in this fashion until deposition is complete; again, all layers are dried prior to follow on operations.

Prior to lamination all previous tape processing operations occur in parallel with yield fallout limited to respective layer types. The lamination operation requires the collation and marriage of parallel processed layers into series of independent wafers. Individual layers, (layers 1,2,3, . . . n), are sequentially placed upon a lamination caul plate; registration is maintained through common tooling which resides in all product layers. The collated wafer stack is vacuum packaged and placed in an isostatic work cell which provides time, temperature, and pressure to yield a leathery wafer structure.

Laminated wafers are placed on firing setters and are loaded onto a belt furnace for product densification. Firing is performed in a single work cell which performs two independent tasks. The primary operation calls for the burning off of solvents and binders which had allowed the tape to remain pliable during the via formation, filling,

conductor deposition, and lamination operations. This binder burnout occurs in the 350–450 C. range. The wafer continues to travel down the belt furnace and enters the peak firing zone where crystallization, and product densification occurs; temperatures ranging to 850–860 C. are typical. Upon cool down the wafers exit the furnace as a homogeneous structure exhibiting asfired conditions. All product firing occurs in an air environment. Post firing operations would not require wafers to be processed through an additional binder burnout steps but would only require exposure to the 850 C. densification temperatures.

Continuity net list testing is performed on individual circuits in wafer form. Net list data files are Ethernet down loaded to the net probe work center and are exercised against respective wafer designs. Opens and shorts testing of embedded nets, and capacitance and resistive load material measurements defines the bulk work center output. Failures are root caused to specific net paths.

Net list tested wafers typically exhibit individual circuit step/repeat patterns which can range from one to fifty or more on any one particular wafer. Conventional diamond saw dicing techniques are employed to singulate and dice circuits out of the net list tested wafers. Common fixturing is in place to handle both 5" and 7" fired wafer formats.

Referring to FIGS. 8 and 8A, in which like elements are provided having like reference designations, a vehicle **250**, here shown as an automobile, has a pair of radar displays **252, 254**, for example lights or LEDs, mounted to a surface of a rear window **256** of the automobile **250**. In this particular embodiment, the displays **252, 254** are disposed on an inner surface of the rear window **256**. The radar displays are coupled to portable radar sensors **258, 260**. In one particular embodiment, the radar displays **252, 254** are coupled sensors **258, 260** via respective ones of wires **262, 264**. In other embodiments, however, a wireless connection can be used between the displays **252, 254** and sensors **258, 260**. The radar sensors **258, 260** may be provided, for example, as the types described above in conjunction with FIGS. 1–7 and/or as described in co-pending U.S. patent application Ser. No. 09/931,276, filed Aug. 16, 2001, and entitled Portable Object Detection System, assigned to the assignee of the present invention and hereby incorporated herein by reference in its entirety.

The radar sensors **258, 260** are each portably mounted to the interior surface of the side windows **266, 268**. The radar sensors **252, 254** can be mounted to window brackets or can be mounted directly on the windows **266, 268**. Wires **270, 272** couple respective ones of the radar sensors **258, 260** to a power source (not shown) such as a car battery or other power source provided as part of the vehicle **250**. It should be appreciated, however, that alternative power sources, such as rechargeable or non-rechargeable batteries, can also be used to provide power to the sensor.

In operation, if one of sensors **258, 260** detects an object within its detection zone, the sensor causes the corresponding display **252, 254** to provide an indication that a sensor has detected an object in its detection zone. An operator of the vehicle **250** receives the indication, via a conventional rear view mirror **274** in which the operator can see radar displays **252, 254**. In this manner, the detection system alerts the operator of the vehicle to the presence of the object within the detection zone associated with each radar sensor **258, 260**.

Alternatively, or in addition to visual indications provided by the displays **252, 253**, the sensors **258, 260** can provide an audible indication of a detected object with an audible

alert device. Though not shown in the figure, it will be recognized by one of ordinary skill in the art that the audible indication can be provided by an audible alert device within the radar displays **252**, **254**, or the radar sensors **258**, **260** or with a separate audible alert device. In some embodiments, it may be desirable, or even necessary to utilize only an audible alert device and in this case, the radar displays **252**, **254** are optional.

Although two radar systems and two displays are here shown and described, it should be appreciated that fewer or more than two radar systems and displays can also be used. The particular number of radar systems and displays to use in any particular application is selected in accordance with a variety of factors including but not limited to the size and shape of the vehicle, the number of blind spots on the vehicle and the location of vehicle blind spots. Also, it will be recognized that in some embodiments, two or more radar systems may be mutually coupled to one radar display. Likewise one, two, or more displays can be coupled to a single radar sensor. Furthermore, while the illustrative embodiment shows the radar system disposed internal to the vehicle **250**, on the interior surface or the side windows, the radar system could also be disposed external to the vehicle, for example on the exterior surface of the side windows.

Referring now to FIG. 9 in which like elements of FIGS. 8 and 8A are provided having like reference designations, the portable sensor **258** is shown to include a housing **270** having first and second opposing surfaces **270a**, **270b**. An antenna system (not visible in FIG. 9) radiates RF energy through the first surface **270a** of the housing **270**. Disposed in the housing **270** are one or more radiating sensor elements provided as part of a highly integrated millimeter wave (MMW) substrate. Disposed on the housing **270** is an audio output port **274** for an audio detection alert, and audio alert on/off switch **276**, a display connector **278** for attachment of a radar display cable, a battery port **280** for attachment of batteries in the alternative power arrangement, and a connector **282** for attachment of vehicle power logic and other signals. The LED **252** is coupled to the sensor **258** via an electrical connection **262**.

RF energy **282** radiates through the face **270a** to detect objects. The sensor **258** can be mounted to a vehicle via a variety of techniques. As explained above in conjunction with FIGS. 1 and 1A, for example, the sensor can be mounted internally to or behind to a portion of the vehicle (e.g. including but not limited to under the vehicle body or skin or shell or cover or behind a vehicle bumper, side panel and vehicle fascia). Also, the sensor can be mounted externally to the vehicle. As shown in FIG. 9, for example, a clip **284** couples the sensor **258** to an inner surface **286a** of an vehicle window **286**. In alternate embodiment, the sensor **258** may be coupled to outer window surface **286b**. The sensor **258** may be, for example, coupled with a hook and loop fastener system generally denoted **288**. The illustrative clip **284** is placed over a top edge of the window **286** of the vehicle and the radar sensor **258** is attached to the clip **284** with hook and loop fasteners **288**. In this manner, sensor **258** is removably coupled and thus portably mounted to the vehicle.

An illustrative sensor **258** is provided having a length L of 12.7 cm, a width W of 7.6 cm and a thickness T of 3.8 cm where the thickness corresponds to the distance between the two surfaces **272a**, **272b**. It will be recognized by one of ordinary skill in the art that sensor systems with other dimensions can also be used. It will be further recognized that other external mounting structures and techniques in addition to the clip **284** are possible.

It will be further recognized by one of ordinary skill in the art that other techniques in addition to the connector **282** can be used to provide power to the sensor **258**. It will be further recognized by one of ordinary skill in the art that the sensor **258** can be mounted to any window or to any interior or exterior surface of the vehicle, so long as the radiating face **272a** is not placed behind a surface through which radar energy cannot propagate effectively. Furthermore, it should be understood that it is necessary to orient the sensor **258** in a particular direction to provide a preferred detection zone about the vehicle.

Having described the preferred embodiments of the invention, it will now become apparent to one of ordinary skill in the art that other embodiments incorporating their concepts may be used. It is felt therefore that these embodiments should not be limited to disclosed embodiments but rather should be limited only by the spirit and scope of the appended claims.

All publications and references cited herein are expressly incorporated herein by reference in their entirety.

What is claimed is:

1. A radar sensor comprising:

- a housing having a base portion and a cover portion;
- a first substrate having first and second opposing surfaces; said first substrate disposed in the base portion of said housing;
- an antenna disposed on the first surface of said first substrate, said antenna having an antenna aperture disposed to radiate through a portion of the base portion of said housing;
- an RF transmit circuit disposed on the second surface of said first substrate, said RF transmit circuit coupled to said antenna;
- an RF receiver circuit disposed on the second surface of said first substrate, said RF receiver circuit coupled to said antenna;
- a second substrate disposed in the base portion of said housing above said first substrate, said second substrate having first and second opposing surfaces;
- one or more IF circuit components disposed on a first one of the first and second opposing surfaces of said second substrate,
- means for coupling at least one of the RF transmit and RF receiver circuits to at least one said one or more IF circuit components; and
- an EMI shield disposed over said first and second substrates to reduce the amount of EMI radiated from the sensor.

2. The sensor of claim 1 wherein said first substrate comprises a low temperature co-fired ceramic (LTCC) substrate.

3. The sensor of claim 2 wherein the LTCC substrate comprises a plurality of layers comprising LTCC tape, each of the plurality of layers coupled to a corresponding one of the plurality of layers by corresponding ones of a plurality of conductive vias.

4. The sensor of claim 3 wherein said antenna is comprised of a plurality of antenna elements, each of said plurality of antenna elements provided from resonant structures formed by conductive vias embedded in said plurality of tape layers.

5. The sensor of claim 4 wherein said second substrate comprises a printed circuit board (PCB).

6. The sensor of claim 5 wherein said means for coupling circuits to the IF circuit components comprises a flex circuit.

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7. A radar sensor comprising:

a housing having:

a base portion having integral sides and an internal surface;

a first support structure disposed on the integral sides;

a second support structure disposed on the base portion;

a first substrate having first and second opposing surfaces, said first substrate disposed on the first support structure and spaced apart from the internal surface by a predetermined distance;

an antenna disposed on the first surface of said first substrate, the antenna having an aperture arranged to radiate through a portion of the base portion of said housing;

an RF transmit circuit disposed on the second surface of said first substrate and coupled to said antenna;

an RF receiver circuit disposed on the second surface of said first substrate, said RF receiver circuit coupled to said antenna;

a second substrate disposed on the second support structure in the base portion of said housing said second substrate having first and second opposing surfaces with the first surface of said second substrate spaced apart from the second surface of said first substrate by a predetermined distance; and

one or more IF circuit components disposed on a first one of the first and second surfaces of said second substrate with at least one of said one or more IF circuit components coupled to at least one of said RF transmit circuit and said RF receiver circuit.

8. The sensor of claim 7 wherein the first support structure comprises a shoulder region disposed on the integral sides of the base portion for supporting said first substrate.

9. The sensor of claim 7 wherein the second support structure comprises a plurality of posts projecting from a bottom portion of the base portion.

10. The sensor of claim 7 further comprising a flex circuit for coupling the transmit and receiver circuits to the IF circuit components disposed on said second substrate.

11. The sensor of claim 7 further comprising a cover disposed on said housing.

12. The sensor of claim 11 wherein the cover is provided having a thickness selected to allow attachment to the base portion via a vibrational technique.

13. The sensor of claim 7 further comprising a radome disposed about the antenna aperture to tune the antenna.

14. The sensor of claim 7 wherein said antenna is comprised of a plurality of antenna elements, each of said plurality of antenna elements provided from resonant structures formed by conductive vias embedded in said plurality of tape layers.

15. The sensor of claim 14 wherein:

said RF transmit circuit is provided as a monolithic microwave integrated circuit;

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said RF receiver circuit is provided as a monolithic microwave integrated circuit; and

said IF circuit comprises at least one discrete circuit component.

16. The sensor of claim 15 further comprising an electronics portion disposed on said second substrate and coupled to at least one of said one or more IF circuit components, the electronics portion comprising:

a digital signal processor (DSP);

a digital to analog converter (DAC);

a power supply;

a local area network transceiver and controller;

an analog to digital converter (A/D); and

a voltage controlled oscillator (VCO).

17. The sensor of claim 16 wherein the housing further comprises an EMI shield disposed over said first and second substrates for reducing the amount of EMI radiated from the sensor.

18. The sensor of claim 14 further comprising one or more of the plurality of tape layers.

19. The sensor of claim 7 wherein at least one of said RF transmitter circuit and said RF receiver circuit are provided as monolithic microwave integrated circuits (MMICs).

20. The sensor of claim 7 further comprising:

an audio output circuit having a first port at which is provided an audio detection alert;

an audio alert on/off switch coupled to said audio output circuit;

a display connector for attaching a radar display cable;

a battery port adapted to couple at least one battery; and

a connector for attaching a vehicle power and logic signal cable.

21. A radar sensor comprising:

a housing having an internal surface and a first support structure and a second support structure disposed thereon;

a first substrate comprising a plurality of low temperature co-fired ceramic (LTCC) layers, said first substrate disposed on the first support structure and spaced apart from the internal surface by a predetermined distance,

an antenna provided from the LTCC layers;

an RF transmitter circuit provided in the LTCC layers;

an RF receiver circuit provided in the LTCC layers;

a second substrate disposed on the second support structure and spaced above said first substrate by a predetermined distance; and

an IF circuit disposed on the second substrate.

22. The sensor of claim 21 further comprising a plurality of conductive vias provided in the LTCC layers, said conductive vias for interconnecting said antenna to said RF receiver and RF transmitter circuits.

\* \* \* \* \*

UNITED STATES PATENT AND TRADEMARK OFFICE  
**CERTIFICATE OF CORRECTION**

PATENT NO. : 6,501,415 B1  
DATED : December 31, 2002  
INVENTOR(S) : Luis M. Viana et al.

Page 1 of 1

It is certified that error appears in the above-identified patent and that said Letters Patent is hereby corrected as shown below:

Column 2,

Line 66, reads "and RF antenna" and should read -- an RF antenna, --.

Column 3,

Line 5, reads "of shown" and should read -- of the type shown --.

Line 27, reads "or other vehicle portion" and should read -- or other vehicle portions --.

Line 33, reads "The radar systems 10" and should read -- The radar system 10 --.

Line 44, reads "The radar systems 10 are each" and should read -- The radar system 10 can be --.

Line 45, reads "section 12" and should read -- section 12, which is --.

Line 45, reads "which allows" and should read -- that allows --.

Column 5,

Line 23, reads "is disposed is the" and should read -- is disposed in the --.

Column 10,

Line 9, reads "through an additional" and should read -- through additional --.

Column 11,

Line 34, reads "and audio alert" and should read -- an audio alert --.

Line 50, reads "of an" and should read -- of a --.

Column 12,

Line 46, reads "one said one or" and should read -- one of said one or --.

Column 13,

Line 23, reads "opposing: surfaces" and should read -- opposing surfaces --.

Signed and Sealed this

Thirteenth Day of May, 2003

A handwritten signature in black ink, appearing to read "James E. Rogan", with a horizontal line drawn underneath it.

JAMES E. ROGAN  
*Director of the United States Patent and Trademark Office*