



US008477065B2

(12) **United States Patent**
Barrick et al.

(10) **Patent No.:** **US 8,477,065 B2**
(45) **Date of Patent:** **Jul. 2, 2013**

(54) **COMBINED TRANSMIT/RECEIVE
SINGLE-POST ANTENNA FOR HF/VHF
RADAR**

343/855, 866–871, 874, 875, 700 R, 718;
455/403, 404.1

See application file for complete search history.

(75) Inventors: **Donald E. Barrick**, Redwood City, CA
(US); **Peter M. Lilleboe**, San Jose, CA
(US)

(56)

References Cited

U.S. PATENT DOCUMENTS

1,839,290	A *	1/1932	Bailey	342/436
2,256,619	A *	9/1941	Luck	343/726
2,392,328	A *	1/1946	Lear	342/423
2,401,565	A *	6/1946	Holmes	342/420
2,468,116	A *	4/1949	Schaeffer	342/429
2,586,342	A *	2/1952	Jarvis	342/434
2,994,031	A *	7/1961	Slattery	342/22
3,005,197	A *	10/1961	Shearer	342/465
3,261,017	A *	7/1966	Luftig	342/465
3,344,430	A *	9/1967	Hildebrand	342/437

(Continued)

(73) Assignee: **CODAR Ocean Sensors Ltd**, Mountain
View, CA (US)

(*) Notice: Subject to any disclaimer, the term of this
patent is extended or adjusted under 35
U.S.C. 154(b) by 155 days.

(21) Appl. No.: **13/223,128**

(22) Filed: **Aug. 31, 2011**

(65) **Prior Publication Data**

US 2011/0309973 A1 Dec. 22, 2011

Related U.S. Application Data

(63) Continuation of application No. 12/505,093, filed on
Jul. 17, 2009, now Pat. No. 8,031,109.

(51) **Int. Cl.**
G01S 7/02 (2006.01)
H01Q 7/00 (2006.01)
G01S 13/00 (2006.01)

(52) **U.S. Cl.**
USPC **342/175**; 342/82; 342/89; 343/725;
343/728; 343/741; 343/866; 343/867; 343/874

(58) **Field of Classification Search**
USPC 342/27, 59, 82, 89, 90, 104, 118,
342/125, 165, 175, 22, 26 R–26 D, 350, 351,
342/385, 417, 419, 420, 422, 423, 424, 428,
342/429, 432, 433, 434, 436, 437, 441, 442,
342/444, 448, 450, 460, 463, 464, 465; 343/722,
343/725, 726, 728, 729, 731, 732, 741–745,
343/748, 757, 763, 764, 787, 788, 850, 853,

OTHER PUBLICATIONS

US Notice of Allowance dated Jun. 14, 2011 for U.S. Appl. No.
12/505,093.

Primary Examiner — Bernarr Gregory

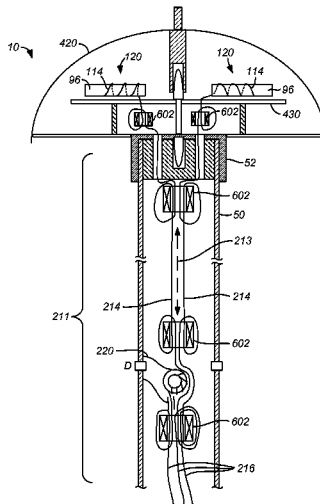
(74) *Attorney, Agent, or Firm* — Weaver Austin Villeneuve
& Sampson, LLP

(57)

ABSTRACT

An antenna configuration is described for high frequency (HF) or very high frequency (VHF) radars contained in a single vertical post. The radar may include a vertical dipole or monopole transmitting antenna collocated with a three-element receive antenna. The three antennas including two crossed loops and a vertical element are used in a direction-finding (DF) mode. Isolation between the three antennas produces high quality patterns useful for determining target bearings in DF mode. The single vertical post is sufficiently rigid mechanically that it may be installed along a coast without guy wires.

20 Claims, 6 Drawing Sheets



U.S. PATENT DOCUMENTS

3,701,155	A *	10/1972	Adams	342/423	5,361,072	A	11/1994	Barrick et al.	
4,054,881	A *	10/1977	Raab	342/448	5,552,796	A *	9/1996	Diamond	343/742
4,121,216	A *	10/1978	Bunch et al.	342/424	5,945,947	A *	8/1999	Cunningham	342/442
4,135,191	A *	1/1979	Sawicki	342/436	6,484,021	B1 *	11/2002	Hereford et al.	455/404.1
4,194,207	A *	3/1980	Zauscher	342/434	6,774,837	B2	8/2004	Barrick et al.	
4,194,244	A *	3/1980	Lewis	342/444	6,822,574	B2 *	11/2004	Nakamura	342/460
4,302,759	A *	11/1981	Mori et al.	342/436	6,856,276	B2	2/2005	Barrick et al.	
4,306,240	A *	12/1981	Yasuda et al.	342/436	6,919,839	B1	7/2005	Beadle et al.	
4,307,402	A *	12/1981	Watanabe	342/433	6,963,301	B2	11/2005	Schantz et al.	
4,314,251	A *	2/1982	Raab	342/463	7,298,314	B2	11/2007	Schantz et al.	
4,433,336	A *	2/1984	Carr	343/728	7,414,571	B2	8/2008	Schantz et al.	
4,489,327	A *	12/1984	Eastwell	342/433	7,538,715	B2	5/2009	Langford et al.	
4,528,566	A *	7/1985	Tyler	342/419	7,592,949	B2	9/2009	Schantz et al.	
4,573,053	A *	2/1986	Mori et al.	342/441	7,688,251	B2	3/2010	Barrick et al.	
4,588,993	A *	5/1986	Babij et al.	342/351	7,755,552	B2 *	7/2010	Schantz et al.	343/718
4,595,928	A *	6/1986	Wingard	343/742	7,859,452	B2	12/2010	Schantz et al.	
4,724,442	A *	2/1988	King	342/434	2006/0132352	A1	6/2006	Schantz et al.	
4,806,851	A *	2/1989	Krider et al.	342/460					

* cited by examiner

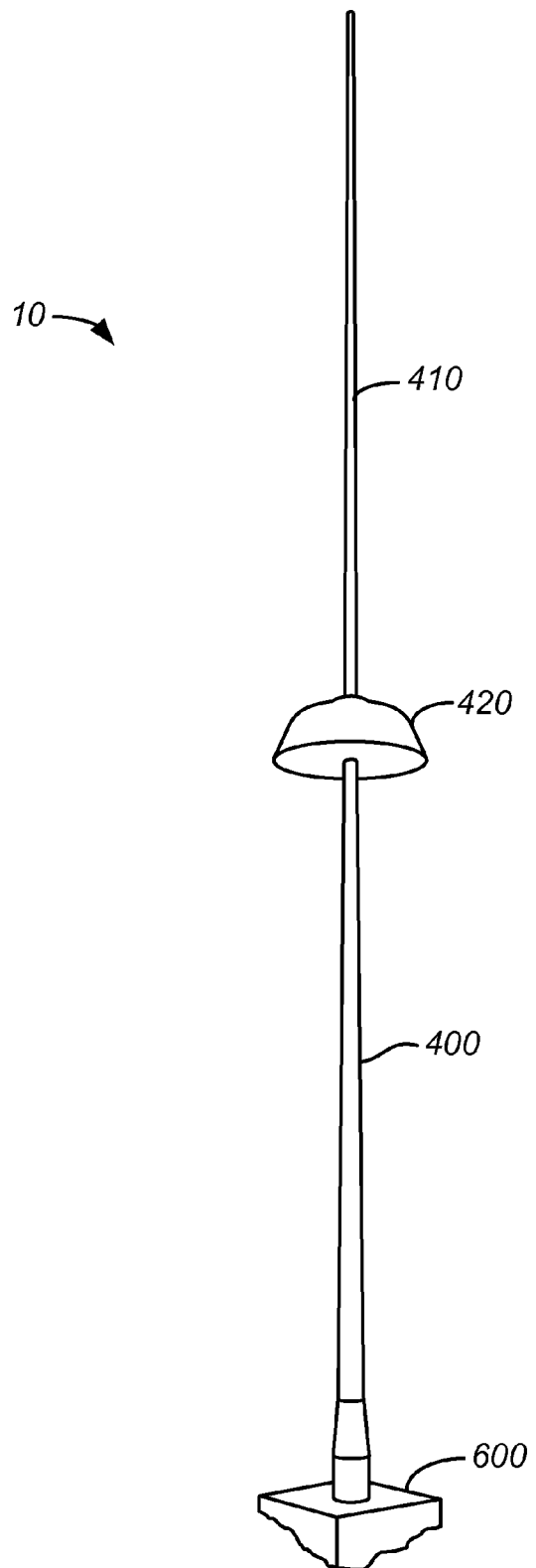


FIG. 1

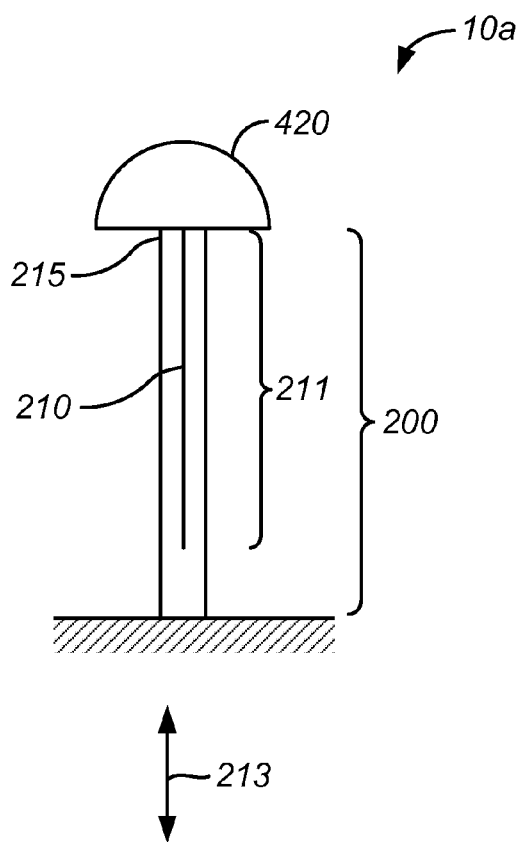


FIG. 2A

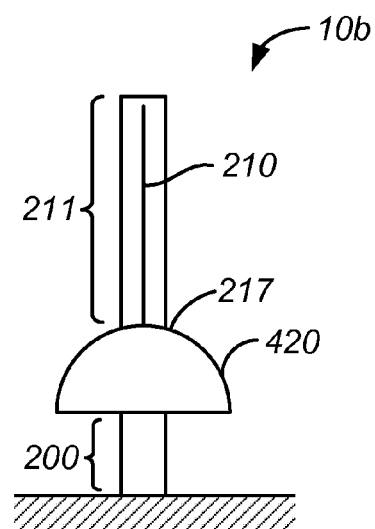
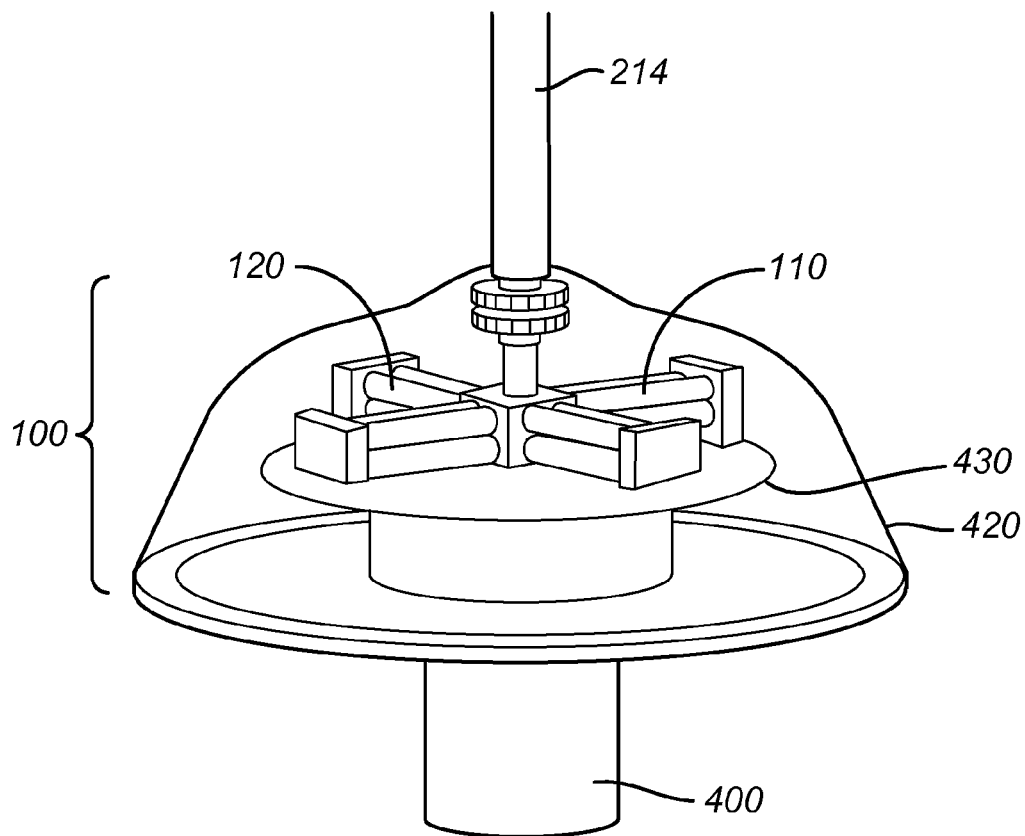


FIG. 2B

**FIG. 3**

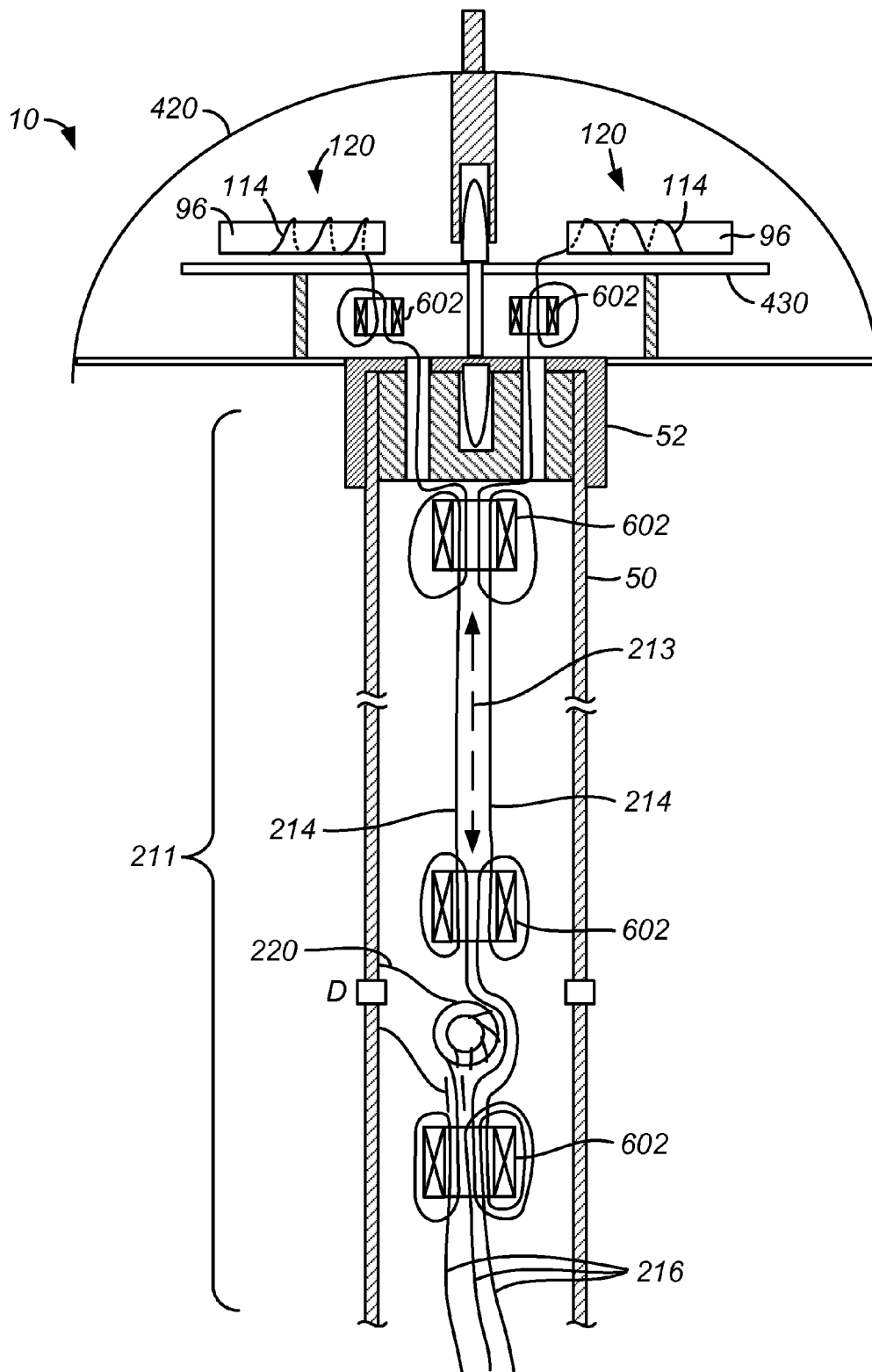


FIG. 4

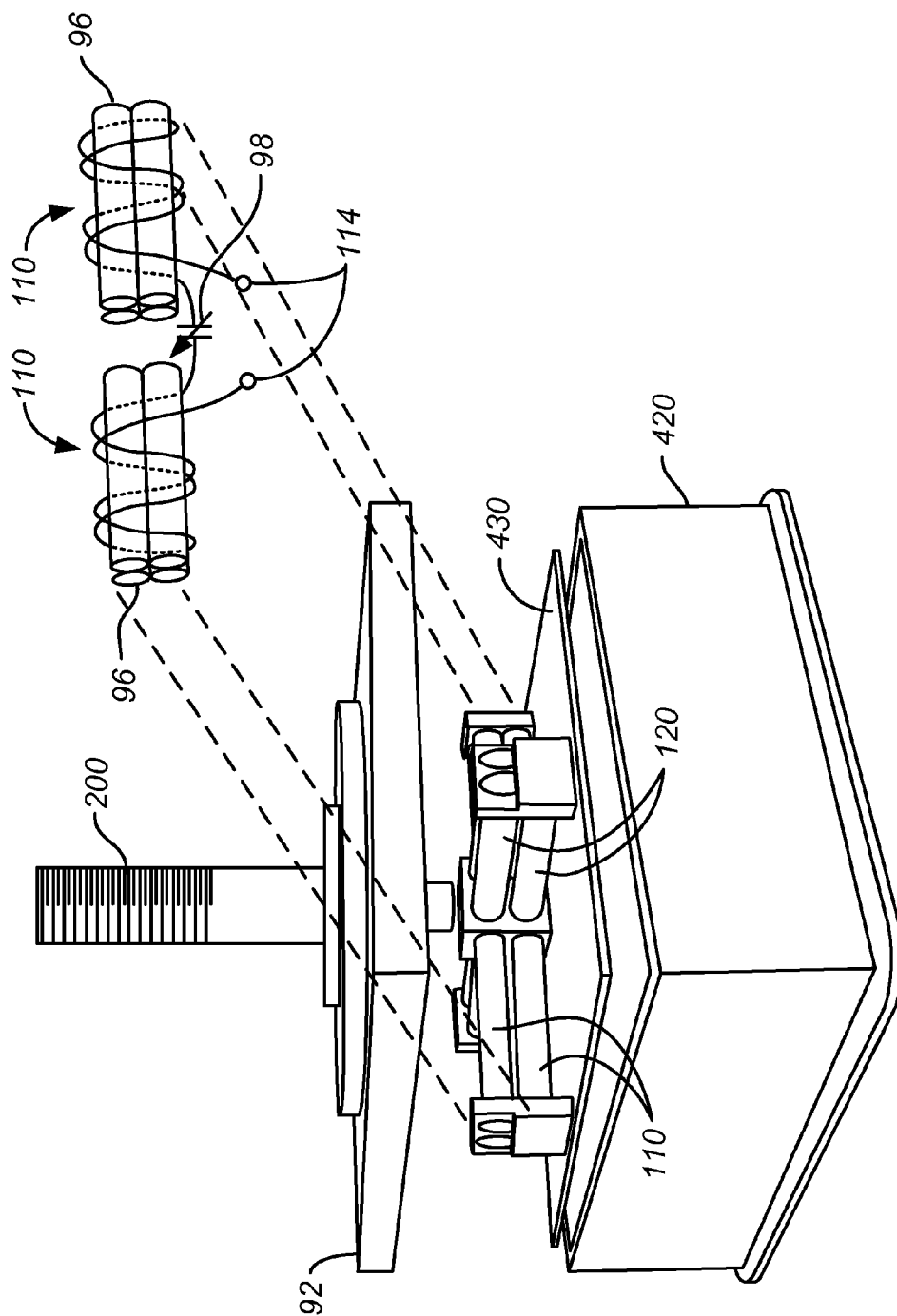


FIG. 5

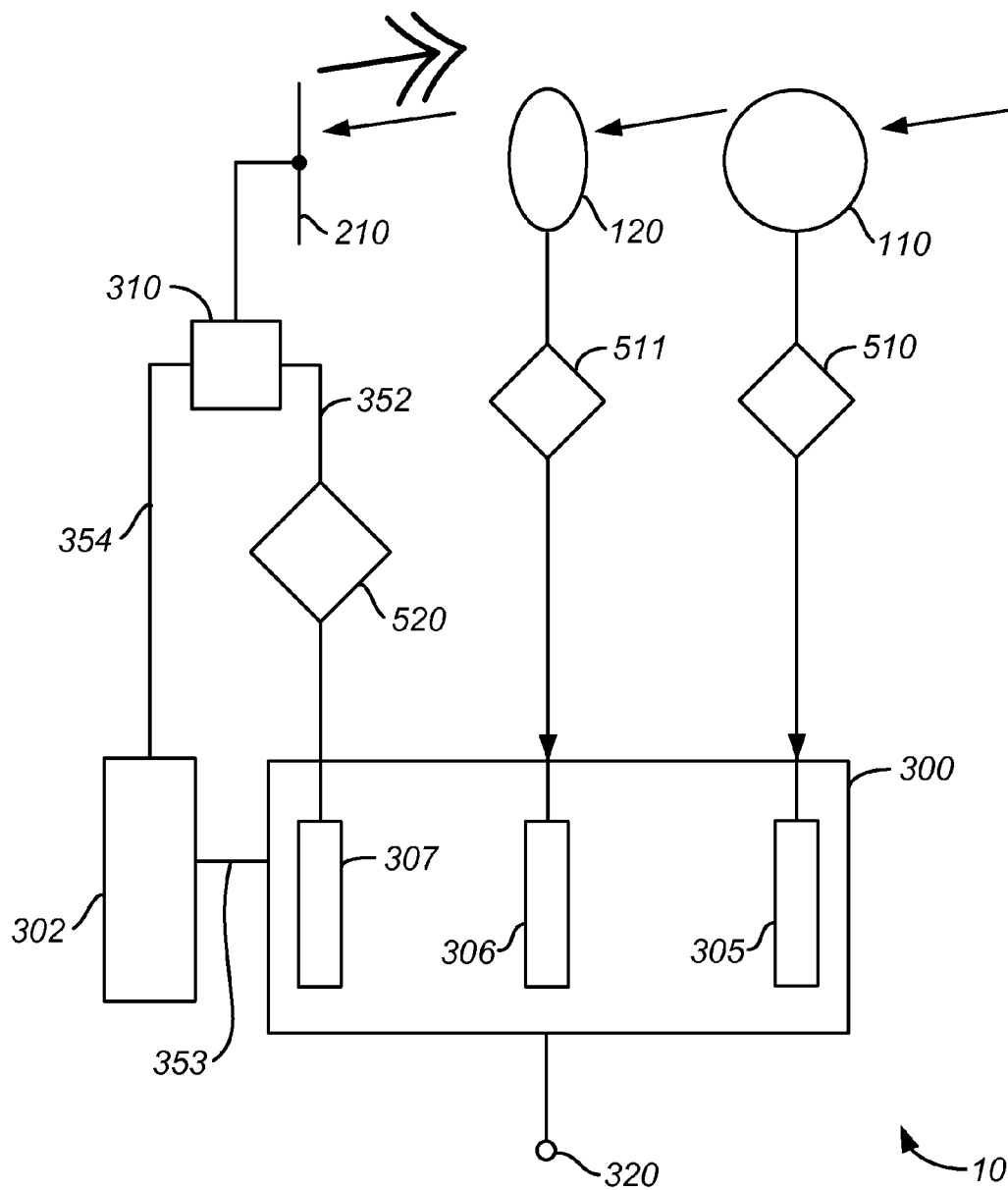


FIG. 6

1

COMBINED TRANSMIT/RECEIVE SINGLE-POST ANTENNA FOR HF/VHF RADAR

RELATED APPLICATIONS

This application claims priority under U.S.C. §120 from and is a continuation of U.S. patent application Ser. No. 12/505,093, filed Jul. 17, 2009 and titled "COMBINED TRANSMIT/RECEIVE SINGLE-POST ANTENNA FOR HF/VHF RADAR", which is hereby incorporated by reference, now U.S. Pat. No. 8,031,109.

BACKGROUND

1. Field of the Invention

The present methods, devices, and systems relate generally to the field of radars, and more particularly to HF/VHF radars that scatter signals from ocean surface or from targets such as ships on the sea. Specifically, the present methods, devices, and systems invention relate to antenna systems useful for such radars. The present methods, devices, and systems facilitate reduction in antenna system size while providing the level of performance found in current larger antenna systems.

2. Description of the Related Art

HF radars have been used since the 1960s. When located at coastal areas and transmitting vertical polarization, HF radar systems may exploit the high conductivity of sea water to propagate their signals (e.g., in a surface-wave mode) well beyond the visible or microwave-radar horizon. Although HF surface-wave radar (HFSWR) was initially considered for detecting military targets beyond the horizon (e.g., ships, low-flying aircraft or missiles), HFSWR also found widespread acceptance and use in the mapping of sea surface currents and the monitoring of sea state (e.g., waveheights). The radar echo used in these sea mapping/monitoring applications comes from Bragg scatter by ocean surface waves that are about half the radar wavelength, traveling toward and away from the radar.

Conventional radars determine target bearing by forming and scanning narrow beams using radar antennas. One procedure for sea mapping/monitoring using HFSWR has been to use a transmit antenna system that floodlights a large bearing sector of the sea (e.g., 60°) with illumination. A separate receive phased-array then forms a narrow beam that is scanned across the illuminated sector using software algorithms after signal digitization. The beamwidth (i.e., angular resolution) depends on the length of the antenna aperture, being proportional in radians to the wavelength divided by the array length. Because the wavelength at HF may be almost 1000 times greater than for microwave radars, the length of an HF array may be hundreds of meters long. While such radars were built and operated in the 1960s, antenna size and related cost impeded widespread acceptance. Coastal locations are valuable land for other public and private use, and suitable locations for large antennas as coastal structures are difficult to obtain.

Compact HF radar systems may take the place of the above-described large phased arrays. CODAR systems have employed separate transmit and receive antenna subsystems, with the two units separated by up to a wavelength. In many cases, such structures were still considered to be too obtrusive, and therefore incompatible with public use in beach areas, or for deployment on oil platforms or building rooftops.

These compact antenna systems for sea mapping/monitoring coastal radars included separate transmit and receive antenna subsystems. The transmit unit was usually an omni-

2

directional monopole, and the receive unit consisted of two crossed loops coaxially collocated on a vertical monopole. Such antenna systems were sufficiently compact that they were suitable for mounting on offshore oil platforms and on coastal building rooftops. Reductions in size may be achieved by replacing the large air loops employed by earlier technology with tiny crossed ferrite loopsticks housed in a weather-proof box on the post surrounding the monopole.

The loopstick antennas take advantage of the fact that an inefficient HF receive system will cause reduction of the desired target signal as well as a proportional reduction in the external noise. Therefore a signal to noise ratio (SNR) of the HF receive system may remain constant with decreased efficiency, to the point where the external noise is approaches the internal receiver noise, at which point SNR begins to suffer. Thus, the size and cost of the HF receiver antenna subsystem can be reduced (thereby decreasing its efficiency) to the point that the external noise approaches the internal receiver noise before any SNR penalty is experienced by the HF receiver antenna subsystem.

Coastal space available for radar antenna systems continues to shrink, and further reductions in size are desired. Coupling between transmit and receive antennas in a radar system reduce performance of the radar antenna system. Furthermore, external obstacles nearby such as power lines, buildings, fences, and trees all exacerbate mutual coupling problems.

SUMMARY

According to one aspect of the disclosure, an antenna system can be configured to transmit and receive (e.g., an antenna system that transmits and receives) radar signals includes a compact receive unit configured to receive HF or VHF radar signals. The compact receive unit includes a first loopstick antenna having a first phase center and a first loopstick axis. The compact receive unit also includes a second loopstick antenna having a second phase center and a second loopstick axis. The second loopstick axis is substantially orthogonal to the first loopstick axis. The compact receive unit is disposed within a receive unit enclosure that is hermetically sealed. The antenna system also includes a transmit/receive unit configured to transmit and receive the HF or VHF radar signals. The transmit/receive unit includes a substantially vertical transmit/receive antenna having a transmit/receive phase center. The transmit/receive phase center, the first phase center, and the second phase center are substantially collinear along a substantially vertical axis. A transmit/receive axis of the substantially vertical transmit/receive antenna is substantially orthogonal to the first loopstick axis and to the second loopstick axis. The transmit/receive unit also includes a conducting cylinder enclosing at least a portion of the substantially vertical transmit/receive antenna. The transmit/receive unit further includes at least one decoupling device inside the conducting cylinder and surrounding a portion of the substantially vertical transmit/receive antenna to decouple the substantially vertical transmit/receive antenna from the conducting cylinder and/or from the loopstick antennas. The antenna system also includes a receiver module coupled to the compact receive unit and to the transmit/receive unit. The receiver module is configured to receive a first receiver input signal from the compact receive unit. The receiver module is also configured to receive a second receiver input signal from the transmit/receive unit. The receive module is further configured to output a signal that is amplified and sent to the transmit/receive unit for radiation.

Any embodiment of any of the present methods and systems may consist of or consist essentially of—rather than comprise/include/contain/have—the described functions, steps and/or features. Thus, in any of the claims, the term “consisting of” or “consisting essentially of” may be substituted for any of the open-ended linking verbs recited above, in order to change the scope of a given claim from what it would otherwise be using the open-ended linking verb.

BRIEF DESCRIPTION OF THE DRAWINGS

The following drawings form part of the present specification and are included to further demonstrate certain aspects of the present methods and apparatuses. The drawings illustrate by way of example and not limitation. Identical reference numerals do not necessarily indicate an identical structure. Rather, the same reference numeral may be used to indicate a similar feature or a feature with similar functionality. Not every feature of each embodiment is labeled in every figure in which that embodiment appears, in order to keep the figures clear.

FIG. 1 is an illustration of a combined radar transmit and receive antenna according to one embodiment.

FIG. 2A is a profile view of a combined radar transmit and receive antenna having a receive unit at a top end according to one embodiment.

FIG. 2B is a profile view illustrating a combined radar transmit and receive antenna having a receive unit at a bottom end according to one embodiment.

FIG. 3 is a cross-sectional view illustrating a receive unit according to one embodiment.

FIG. 4 is a cross-sectional view illustrating an antenna system according to one embodiment.

FIG. 5 is a block diagram illustrating a three element collocated crossed-loopstick and monopole receive antenna unit according to one embodiment.

FIG. 6 is a block diagram illustrating a combined radar transmit and receive antenna according to one embodiment.

DESCRIPTION OF ILLUSTRATIVE EMBODIMENTS

The terms “comprise” (and any form of comprise, such as “comprises” and “comprising”), “have” (and any form of have, such as “has” and “having”), “include” (and any form of include, such as “includes” and “including”) and “contain” (and any form of contain, such as “contains” and “containing”) are open-ended linking verbs. Thus, a method comprising certain steps is a method that includes at least the recited steps, but is not limited to only possessing the recited steps. Likewise, a device or system comprising certain elements includes at least the recited elements, but is not limited to only possessing the recited elements.

The terms “a” and “an” are defined as one or more than one, unless this application expressly requires otherwise. The term “coupled” is defined as connected, although not necessarily directly, and not necessarily mechanically.

A difference in efficiency between transmit and receive antennas may influence sensitivity to coupling. Improved transmit antenna efficiency is obtained at vertical sizes between a quarter and a half wavelength. Currents may be induced on such antennas at or near resonance. On the other hand, inefficient loop antennas may be used for receive antennas because they are compact and low cost. Loop antennas may have low radiative current flow. As a result, the efficient

element with high currents represents an unbalance when physically located near the inefficient antenna with small currents.

A slight perturbation in a current on the transmit antenna may be bigger than a current on the receive antenna. This small perturbation may be produced by some dissymmetry with the loop antennas, feed lines, or from nearby metallic or dielectric obstacles that are often unavoidable. The transmit antenna current perturbation induces a weak current on the loop antenna that disrupts received signals. Thus, the transmit antenna is coupled to the loop antenna resulting in disrupted signals at the loop antenna. Coupling may be calculated according to the equation given below.

$$\text{Coupling} = \text{loop/dipole inefficiency} + \text{loop/dipole isolation (dB)}$$

Both the loop/dipole inefficiency quantity and the loop/dipole isolation quantity are negative numbers. The coupling may be measured with a network analyzer as the ratio of the measured current out of the loop to the current into the dipole (or monopole). The output current from the loop includes gain from preamplifiers. According to one embodiment, loop/dipole isolation for acceptable received loop antenna patterns may be 20 dB.

For example, at 12-14 MHz the loop/dipole inefficiency ratio may be -10 to -12 dB. This includes loop antenna preamplifier gain, which may be 20 dB. Without the preamplifier the inefficiency may be -30 to -32 dB. Based on the above equation, according to one embodiment, a coupling level may be -30 to -32 dB for 12-14 MHz. The difference in efficiencies may grow (decrease) as the frequency is reduced (raised). For another example, at 4-5 MHz an inefficiency ratio may be -20 to -22 dB, and coupling may be -40 to -42 dB. In a further example, at 24-27 MHz an inefficiency ratio may be -5 dB and coupling may be -25 dB.

An antenna system as described below combines transmit and receive antennas in a small form factor that occupies small land areas and is hermetically sealed against natural elements such as rain. Coupling between the transmit and receive antennas is reduced to allow the transmit and receive antennas to be collocated without distorting the signal patterns received by the antenna system.

FIG. 1 is an illustration of a combined radar transmit and receive antenna according to one embodiment. An antenna system 10 includes a receive unit enclosure 420 attached to a mast 400. The mast 400 is oriented substantially vertical to the ground. The mast 400 may be a conducting tube (e.g., aluminum) through which feed wires run surrounded by a fiberglass tube. A portion of the antenna system 410 above the receive unit enclosure 420 may have a semi-rigid whip structure. The location of the receive unit enclosure 420 on the mast 400 may vary such that the portion of the antenna system 410 extends above the receive unit enclosure 420. According to one embodiment, the receive unit enclosure 420 may be located between about 10 and about 90 percent (e.g., 10, 20, 30, 40, 50, 60, 70, 80, 90 percent) along the length of the mast 400 above a concrete footer 600. For example, the receive unit enclosure 420 may be located half way up the mast 400 from the concrete footer 600.

The receive unit enclosure 420 is hermetically sealed and protected from natural elements such as rain resulting in a watertight and weatherproof structure. The antenna system 10 is mechanically stable by mounting the mast 400, for example, in the concrete footer 600, allowing the antenna system 10 to stand freely without the use of horizontally extending guy wires. Thus, the antenna system 10 occupies a small footprint in coastal land.

5

According to one embodiment the antenna system **10** may operate in high frequency (HF) or very high frequency (VHF) ranges. If a frequency range such as, for example, 12-14 MHz is desired the antenna system **10** may include a dipole antenna. In this frequency range, a height of the antenna system **10** may be one half the wavelength of operation or 60% to 100% of one half the wavelength of operation (e.g., approximately 25 feet). If a frequency range such as, for example, 4-5 MHz is desired the antenna system **10** may include a monopole antenna with radial ground-screen wires lying on the ground or buried slightly beneath the surface. A monopole antenna is generally one half of a dipole antenna and may have a ground plane on the ground. In this frequency range, a height of the antenna system **10** may be one quarter the wavelength of operation or 60% to 100% of one quarter the wavelength of operation.

The dipole or monopole antenna may be housed in the mast **400** and/or the portion **410** and operate as both a transmit and receive antenna. The receive unit enclosure **420** may house additional receive antennas such as, for example, crossed loop antenna elements. The antenna system **10** may receive and process one or more signals.

Coupling between antennas housed in the receive unit enclosure **420**, the mast **400**, and the portion of the antenna system **410** may be reduced by adjusting a location of the receive unit enclosure **420** in the antenna system. Two example locations for the receive unit enclosure **420** are presented in FIGS. 2A-2B.

FIG. 2A is a profile view of a combined radar transmit and receive antenna having a receive unit at a top end according to one embodiment. An antenna system **10a** includes a receive unit enclosure **420** mounted on a top end **215** of a transmit/receive unit **200**. The transmit/receive unit **200** includes a transmit/receive antenna **210**, such as a dipole or monopole, having a length **211**. A transmit/receive axis **213** of the antenna system **10a** is substantially parallel to the transmit/receive antenna **210**.

In this embodiment, antennas located in the receive unit enclosure **420** are positioned at locations where undesired coupling of the antennas in the receive unit enclosure **420** to currents resulting from the transmit/receive antenna **210** are low. Thus, coupling between the transmit/receive antenna **210** and the receive unit enclosure **420** is reduced.

Although the receive unit enclosure **420** is shown on the top end **215**, the receive unit enclosure **420** may be mounted anywhere along the transmit/receive unit **200**. An alternative arrangement of the receive unit enclosure **420** is shown in FIG. 2B.

FIG. 2B is a profile view illustrating a combined radar transmit and receive antenna having a receive unit at a bottom end according to one embodiment. The antenna system **10b** includes the receive unit enclosure **420** mounted above the transmit/receive unit **200**. The transmit/receive antenna **210** having the length **211** is mounted above the receive unit enclosure **420** on a bottom end **217** of the transmit/receive antenna **210**.

Coupling between antennas in the receive unit enclosure **420** and the mast **400** and the portion **410** may be reduced when the receive unit enclosure **420** is located near a bottom end of the antenna system **10b** because coupling with currents from the dipole or monopole antenna are reduced. Additionally, coupling may be reduced through adjusting a feed point of the antenna in the mast **400** and portion **410**. Off-center feeds for antennas provide adjustable matching impedance and tapering of a vertical current distribution to reduce coupling.

6

FIG. 3 is a cross-sectional view illustrating a receive unit according to one embodiment. The receive unit enclosure **420** is mounted on the mast **400** and coupled (e.g., attached) to an upper dipole antenna portion **214**.

The receive unit enclosure **420** has a compact receive unit **100**, which includes a first loopstick antenna **110** collated with a second loopstick antenna **120**. The second loopstick antenna **120** is aligned substantially orthogonal to the first loopstick antenna **110**. Thus, a first loopstick axis or plane is substantially orthogonal to a second loopstick axis or plane. Further, the first loopstick axis and the second loopstick axis are substantially orthogonal to a transmit/receive axis **213** of the transmit/receive unit **200**. The first loopstick antenna **110** has a first phase center, and the second loopstick antenna **120** has a second phase center. The first phase center and the second phase center may be located collinear with or collocated along a substantially vertical axis with a transmit/receive phase center of the transmit/receive unit **200**.

Windings around the loopstick antennas **110**, **120** have a number of turns selected, in part, such that a resonant condition is realized for the frequency band of operation. The resonant condition may also be selected, in part, using a fixed or adjustable tuning capacitance (not shown) in series with the loopstick antennas **110**, **120**. That is, the frequencies of operation of the compact receive unit **100** may be adjusted, in part, through the number of windings of the loopstick antennas **110**, **120** and a tuning capacitance.

The loopstick antennas **110**, **120** may be coupled to feed lines, amplifiers, or preamplifiers through a board **430** such as, for example, a printed circuit board. According to one embodiment, the board **430** may include the electronic components such as, for example, preamplifiers for increasing the magnitude of signal received by the loopstick antennas **110**, **120**. In this embodiment, the loopstick antennas **110**, **120** may be active antennas.

According to one embodiment, the input impedance of the compact receive unit **100** matches feed lines and amplifiers by canceling out the reactive impedance. For example, the input impedance of the compact receive unit **100** may be approximately fifty ohms.

FIG. 4 is a cross-sectional view illustrating an antenna system according to one embodiment. The antenna system **10** has the receive unit enclosure **420** mounted on the transmit/receive unit **200**. The receive unit enclosure **420** includes the first loopstick antenna **110** and the second loopstick antenna (extending out of the page). The loopstick antenna **110** may be, for example, a ferrite rod **96** wrapped with a wire **114**.

The dipole antenna portions **214**, **216** may not include equal number of wires. For example, one wire of the lower dipole antenna portion **216** may couple to a feed point **220**. The feed point is on a conducting cylinder **50**, such as aluminum. The conducting cylinder **50** is encased in a vertical fiberglass cylinder for structural rigidity as well as for protection from weather and other natural elements.

The conducting cylinder **50** carries currents on a surface of the conducting cylinder, and the currents may transmit or receive signals. In the case of the lower dipole antenna portion **216** being a coaxial cable, the currents on the conducting cylinder **50** may induce currents on an outer shield of the lower dipole antenna portion **216**. Currents on the lower dipole antenna portion **216** and the conducting cylinder **50** may couple to create an unsymmetrical radiation pattern. Along the dipole antenna portions **214**, **216** may be one or more decoupling devices such as ferrite filters **602**.

The ferrite filters **602** placed along the lower dipole antenna portion **216** and the upper dipole antenna portion **214** reduce coupling between (decouple) the antenna portions

214, 216 and the conducting cylinder **50** (and/or between the antenna portions **214, 216** and the loopstick antennas) due to the dissymmetry of the feed being placed on one side of the dipole or monopole conducting cylinder.

Each of the ferrite filters **602** may present an impedance to current flow of approximately 50 to 100 ohms. The impedance of each ferrite filter **602** is based, in part, on a number of turns of wire within an inner diameter on the ferrite filter **602**. For example, if three or four turns are used, impedance of the ferrite filter **602** may exceed 500 ohms.

According to one embodiment, several ferrite filters **602** are placed at locations near the feed point **220**. In another embodiment, coupling may be measured while ferrite filters **602** are individually added. When a point of diminishing return is reached such that additional ferrite filters **602** do not reduce coupling, no more ferrite filters **602** are added.

A position of the feed point **220** determines, in part, coupling within the antenna system **10**. According to one embodiment, the feed point **220** is held in a relatively constant location by foam filler (not shown). The foam filler may be placed in several locations to prevent cable position changes of the cables.

The antenna system **10** operates along the transmit/receive axis **213**, which is substantially parallel to the length **211** of the transmit/receive antenna **210**.

FIG. 5 is a block diagram illustrating a three element collocated crossed-loopstick and monopole receive antenna unit according to one embodiment. An embodiment of a three element collocated crossed-loopstick and monopole receive antenna unit is disclosed in U.S. Pat. No. 5,361,072, which is incorporated by reference here. The board **430** is coupled to the first loopstick antenna **110** and the second loopstick antenna **120**. The board **430** may be a printed circuit board and include preamplifiers coupled to the antennas **110, 120**. The first loopstick antenna **110** includes ferrite rods **96** and a wire **114** wrapped around the ferrite rods **96**. A tuning capacitor **98** is coupled between ferrite rods **96**.

According to one embodiment, the antennas **110, 120**, and other antennas have substantially equal signal levels. The material of the ferrite rods **96** and preamplifiers on the board **430** may be selected to optimize a ratio of external noise to internal noise. For example, margins exceeding 10 decibels may be obtained. Larger margins generally do not increase the signal-to-noise ratio (SNR) of the antenna system **10**.

The board **430** and antennas **110, 120** are enclosed in the receive unit enclosure **420** with a weatherproof lid **92**. The transmit/receive unit **200** is attached to the weatherproof lid **92**.

FIG. 6 is a block diagram illustrating a combined high frequency radar transmit and receive antenna according to one embodiment. The antenna system **10** includes a receiver module **300**, which may be, for example, a Direct Digital Synthesizer (DDS) chip. A receiver output signal **353** couples the receiver module **300** to a transmit amplifier **302**. An amplified receiver output signal **354** couples the transmit amplifier **302** to a transmit/receive switch **310**. A second receiver input signal **352** couples the transmit/receive switch **310** to a receiver module channel **307** through a second preamplifier **520**.

The transmit/receive switch **310** switches coupling of a transmit/receive antenna **210** to either receive the second receiver output signal **354** or to provide the second receiver input signal **352**. That is, the transmit/receive switch **310** may control the transmit/receive antenna **210** to transmit the second receiver output signal **354** or receive the second receiver input signal **352**.

According to one embodiment, the transmit/receive switch **310** operates to couple the second receiver input signal **352** to the transmit/receive antenna **210** fifty percent (half) of the time. During the remaining fifty percent (half) of the time the transmit/receive switch **310** operates to couple the transmit/receive antenna **210** to the amplified receiver output signal **354**. The antennas **110, 120** may receive signals one hundred percent of the time. Signals received at the antennas **110, 120, 210** may include reflections from targets illuminated by the antenna **210** (e.g., while the transmit/receive switch **310** couples the transmit/receive antenna **210** to the second receiver input signal **352** such that receiver module channel **307** can receive the second receiver input signal **352**).

The transmit amplifier **302** may increase the magnitude of the receiver output signal **353** to a magnitude appropriate for transmission on the transmit/receive antenna **210**. The transmit amplifier **302** may either be a fixed amplifier or variable controlled through a manual setting or automated controls. The second preamplifier **520** increases the magnitude of the second receiver input signal **352** received from the transmit/receive antenna **210** to a magnitude appropriate for processing in the receiver module **300**. According to one embodiment, the antenna is configured such that during amplification the signal to noise ratio (SNR) of signals being amplified may remain constant.

The transmit/receive antenna **210** may be, for example, a single dipole or monopole antenna, which radiates omnidirectionally to illuminate a sea surface. Additionally a first loopstick antenna **110** and a second loopstick antenna **120** may receive HF or VHF signals. The loopstick antennas **110, 120** are coupled to receiver channel modules **305, 306** of the receiver module **300** through preamplifiers **510, 511**, respectively.

The receiver channel modules **305, 306, 307** inside the receiver module **300** process signals received from the antennas **110, 120, 210**, respectively. Processing may include, for example, demodulation and digitization. A combined digital signal **320** is output from the receiver module **300** and may be coupled to additional components for further processing, storage, or display.

An antenna system as described above has low coupling between the receive antennas and the transmit/receive antenna. Reduced coupling results in more ideal antenna patterns such as, for example, cosine/sine patterns for the loopstick antennas and omni-directional patterns for the dipole or monopole antenna. Additionally, efficiency of the dipole or monopole antenna increases and adequate bandwidth is obtained for the spectral width of desired radar signals. Further, the size and cost of the antenna system is reduced by lowering visible obtrusiveness and allowing structure robustness.

Descriptions of well known assembly techniques, components, and equipment have been omitted so as not to unnecessarily obscure the present methods, apparatuses, an systems in unnecessary detail. The descriptions of the present methods and apparatuses are exemplary and non-limiting. Certain substitutions, modifications, additions and/or rearrangements falling within the scope of the claims, but not explicitly listed in this disclosure, may become apparent to those of ordinary skill in the art based on this disclosure.

The appended claims are not to be interpreted as including means-plus-function limitations, unless such a limitation is explicitly recited in a given claim using the phrase(s) "means for" and/or "step for," respectively.

9

What is claimed is:

1. An antenna system comprising:
a first unit configured to receive HF or VHF radar signals,
the first unit including:
a first loopstick antenna including a first phase center
and a first loopstick axis; and
a second loopstick antenna including a second phase
center and a second loopstick axis that is substantially
orthogonal to the first loopstick axis;
a second unit configured to transmit and receive HF or VHF
radar signals, the second unit including:
a first antenna including a third phase center, wherein the
third phase center, the first phase center, and the sec-
ond phase center are substantially collinear, the first
antenna further including a first axis that is substan-
tially orthogonal to the first loopstick axis and to the
second loopstick axis; and
a receiver module coupled to the first unit and to the second
unit, the receiver module being configured to:
receive a first receiver input signal from the first unit;
receive a second receiver input signal from the second
unit; and
output a receiver output signal to the second unit.
2. The antenna system of claim 1, wherein the first antenna
is a substantially vertical antenna.
3. The antenna system of claim 1, wherein the first unit is
disposed within an enclosure.
4. The antenna system of claim 1, wherein the second unit
further comprises:
a conducting cylinder enclosing a first portion of the first
antenna.
5. The antenna system of claim 4, wherein the second unit
further comprises:
a decoupling device inside the conducting cylinder and
surrounding a second portion of the first antenna,
wherein the decoupling device is configured to decouple
the first antenna from the conducting cylinder, the first
loopstick antenna, and the second loopstick antenna.
6. The antenna system of claim 1, wherein the first antenna
is a dipole antenna or a monopole antenna.
7. The antenna system of claim 1, further comprising a
substantially vertically oriented mast configured to structur-
ally support a portion of the antenna system.
8. The antenna system of claim 1, further comprising:
a first preamplifier configured to amplify the first receiver
input signal by a first gain prior to the first receiver input
signal being received by the receiver module.
9. The antenna system of claim 8, wherein the antenna
system is configured such that the second receiver input sig-
nal is unamplified prior to being received by the receiver
module.
10. The antenna system of claim 9, further comprising:
a second preamplifier configured to amplify the second
receiver input signal by a second gain prior to the second
receiver input signal being received by the receiver mod-
ule, wherein the second gain is different from the first
gain.
11. The antenna system of claim 1, wherein the first loop-
stick antenna comprises a first core and a first wire having a
first length and configured to form multiple turns around the
first core, wherein the second loopstick antenna comprises a
second core and a second wire having a second length and
configured to form multiple turns around the second core, and
wherein the first length and the second length are less than
about one tenth of a wavelength of the HF or VHF radar
signals.

10

12. An antenna system comprising:
a first unit configured to receive HF or VHF radar signals,
the first unit including:
a first loopstick antenna including a first phase center
and a first loopstick axis; and
a second loopstick antenna including a second phase
center and a second loopstick axis that is substantially
orthogonal to the first loopstick axis;
a second unit configured to transmit and receive HF or VHF
radar signals, the second unit including:
a first antenna including a third phase center, wherein the
third phase center, the first phase center, and the sec-
ond phase center are substantially collinear along a
substantially vertical axis, the first antenna further
including a first axis that is substantially orthogonal to
the first loopstick axis and to the second loopstick
axis;
a conducting cylinder enclosing a first portion of the first
antenna; and
a decoupling device inside the conducting cylinder and
surrounding a second portion of the first antenna,
wherein the decoupling device is configured to
decouple the first antenna from the conducting cylin-
der, the first loopstick antenna, and the second loop-
stick antenna; and
a receiver module coupled to the first unit and to the second
unit, the receiver module being configured to:
receive a first receiver input signal from the first unit;
receive a second receiver input signal from the first unit;
and
output a receiver output signal to the second unit.
13. The antenna system of claim 12, wherein the first
antenna is a substantially vertical antenna.
14. The antenna system of claim 12, wherein the first unit
is disposed within an enclosure.
15. The antenna system of claim 12, wherein the first
antenna is a dipole antenna or a monopole antenna.
16. An antenna system comprising:
a first unit configured to receive HF or VHF radar signals,
the first unit including:
a first loopstick antenna including a first phase center, a
first loopstick axis, a first core, and a first wire con-
figured to form multiple turns around the first core;
and
a second loopstick antenna including a second phase
center, a second loopstick axis that is substantially
orthogonal to the first loopstick axis, a second core,
and a second wire configured to form multiple turns
around the second core;
a second unit configured to transmit and receive HF or VHF
radar signals, the second unit including:
a dipole antenna including a third phase center, wherein
the third phase center, the first phase center, and the
second phase center are substantially collinear, the
dipole antenna further including a first axis that is
substantially orthogonal to the first loopstick axis and
to the second loopstick axis.
17. The antenna system of claim 16, wherein the dipole
antenna has a length, and wherein a length of the first wire and
a length of the second wire are less than or equal to about one
fifth of the length of the dipole antenna.
18. The antenna system of claim 16, wherein the dipole
antenna is a substantially vertical antenna.
19. The antenna system of claim 16, wherein the first unit
is disposed within an enclosure.

20. The antenna system of claim **16**, further comprising:
a receiver module coupled to the first unit and to the second
unit, the receiver module being configured to:
receive a first receiver input signal from the first unit;
receive a second receiver input signal from the first unit; 5
and
output a receiver output signal to the second unit.

* * * * *